

EXHIBIT 71

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**BEFORE THE STATE OF CALIFORNIA
STATE WATER RESOURCES CONTROL BOARD**

11 **IN THE MATTER OF**
12 **ADMINISTRATIVE CIVIL**
 LIABILITY COMPLAINT ISSUED
 AGAINST G. SCOTT FAHEY AND
 SUGAR PINE SPRING WATER, LP

EXPERT WITNESS TESTIMONY OF ROSS R. GRUNWALD

GeoResource Management



December 13, 2015

Mr. Scott Fahey
Sugar Pine Spring Water, LP
2787 Stony Fork Way
Boise, ID 83706

Re: Evaluation of Ground Water Withdrawals to the Sugar Pine Spring Water System

Dear Mr. Fahey,

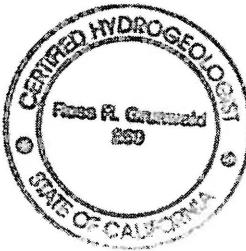
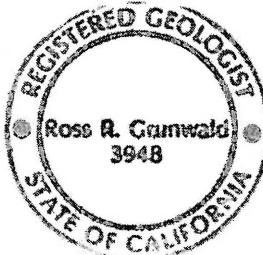
I have been associated with Sugar Pine Spring Water Company since spring of 1996. Development of water collection facilities has evolved over the intervening twenty years. Most recently water flowing to your collection tank was derived from three development wells and two subsurface infiltration galleries installed below the water table at Deadwood, Sugar Pine, Marco and Polo springs.

In my report: "Water Availability Analysis" prepared for and submitted to the Chief, Division of Water Rights, California State Water Resources Control Board, on July 14, 2010, the assumption was made that all of the water extractions from the various components of the system would directly impact the surface spring flow. Thus, the reduction of water volume reporting to the drainage basin would correspond to the total water extracted. However, in reality, this is a worst case scenario and does not relate to the actual case. In fact, water extractions from the various components of the system are much greater than any observed reduction in surface spring flow.

No definitive studies have been made to determine what this difference may be. However, in my professional opinion, the reduction of spring flow is, on average, on the order of 30% of the volume of water removed from the wells and infiltration galleries installed by Sugar Pine Spring Water, LP. Since only 30% of the water withdrawn from system impairs the spring water flows, the remaining 70% is clearly sourced from percolating ground water beneath the site.

The above estimate is based on my experience with the project from its inception in 1996 to the present. A detailed study of water withdrawals and spring flow must be made in order to establish a more definitive ratio between surface flow impairment and withdrawal of percolating ground water. Nevertheless, it is clear that the impairment of surface flow from the springs is much less than that reporting to the Sugar Pine Spring Water, LP, collection system.

Respectfully submitted,



Ross R. Grunwald
California Professional Geologist #3948
California Certified Hydrogeologist #269

Water Availability Analysis Attached

GeoResource Management



**WATER AVAILABILITY
ANALYSIS**

**Prepared for
G. Scott Fahey
Application No. 31491**

**Submitted To:
Chief, Division of Water Rights,
California State Water Resources Control Board**

by
GeoResource Management
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July 14, 2010

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1.0 INTRODUCTION

The purpose of this report is to summarize the results of the water availability analysis conducted for the subject application located within the Hull Creek watershed in Tuolumne County. The objectives of the analysis are as follows:

- To provide information required under California Water Code section 1275 (a), 1375 (d), 1243, 1243.5 and California Code of Regulations, Title 23, section 782, to demonstrate whether water is available for appropriation;
and:
 - To determine the impact of the applications/project on stream flow in order to evaluate potential impacts to Public Trust Resources and provisions for compliance with various federal and state requirements. Examples include the California Environmental Quality Act (CEQA), the California Endangered Species Act (CESA), California Fish and Game Code and the federal Endangered Species Act (ESA).

2.0 PROJECT DESCRIPTION

2.1. Description of the Springs

Marco and Polo Springs, previously unnamed, are located in sections 15 & 22, T 2 N, R 17 E, Monte Diablo Meridian. The longitude and latitude of Marco Spring is: 38.0212 N, 120.0914 W and that of Polo is 38.089 N, 120.0888 W.

Both Marco and Polo Springs are controlled by intersections of northwest-southeast and northeast-southwest trending fractures. The uppermost portions of the springs consist of multiple orifices that issue from areas rather than from a single point (Figures 4 & 6). The springs continue to gain volume as the surface flows continue down toward Hull Creek and reach their maximum flow by the time that they reach the old railroad grade (Figures 4 & 6).

2.2. Proposed Diversions

G. Scott Fahey, proposes to extract a maximum of 20 gallons per minute from each of the springs known as Marco and Polo Springs, located in Tuolumne County, California. This volume equates to a total 32.25 acre-feet annually from each spring. The flow from Marco spring discharges into Hull Creek at a point approximately 0.5 miles upstream from the inflow of Polo spring, when measured along the course of Hull Creek. Hull Creek discharges into the Clavey River approximately 2.5 miles below the inflow of Polo spring. The Clavey River is a Tributary of the Tuolumne River (Figures 2, 3, 4, & 6).

Water withdrawn from these springs will be for human consumption, as sold by various vendors and marketed as bottled spring water.

G. Scott Fahey is currently permitted to draw 14 gallons per minute (22.6 acre-feet/year) of surface flow from each of two springs, Deadwood and Sugar Pine (Application No. 29977, Water Rights Permit 20784). Neither of these springs flow into Hull Creek and are situated on the southeastern and opposite side of the ridge on which both Marco and Polo springs are located (Figure 6).

The natural flow from Deadwood Spring flows southwest into Basin Creek and from there into the North Fork of the Tuolumne River. The natural flow from Sugar Pine Spring flows southwest into Cottonwood Creek and then southeast into the Clavey River.

Withdrawals made from the Tuolumne River basin that are made by Mr. Fahey from Deadwood and Sugar Pine Spring are replaced by water purchased from an out-of-basin source and discharged into the Tuolumne River basin from Phoenix Reservoir. This discharged water flows down Sullivan Creek, into Woods Creek and enters the Tuolumne River at Don Pedro Reservoir. As a result of this water replacement, there is presently no net effect on the Tuolumne River watershed as a whole and there will also be no net effect as a result of the proposed project. The withdrawals from Marco and Polo Springs will only impact the watershed above the Don Pedro Reservoir.

Each of the diversions from Marco and Polo springs will be accomplished by means of subhorizontal wells that will penetrate the root source of each spring to intercept a portion of the spring flow before it reaches the surface. The amount of water flowing from each well will be controlled and monitored at the collar by valves and flow meters. In order to mitigate any effects that these diversions may have during periods of low spring flow, the applicant proposes that these diversions be monitored and regulated in a manner to ensure no less than 2.5 GPM issues from the existing springs' orifices or 20% of the total flow issuing from a spring site, whichever is greater. The amount diverted shall never reduce the surface flow from either spring site by more than 20 GPM

Water flowing from the two developed springs will be conveyed through a pipeline that will be installed along an old railroad grade and introduced into the pipeline that receives the diversions from Sugar Pine spring before those waters will commingle with water from Deadwood Spring. The water will then flow through an existing pipeline to a tank where it will be stored until it is transferred to tanker trucks for transport to a bottling plant.

Figure 1 shows the location of the Hull Creek watershed. Figure 2 shows the Hull Creek drainage basin and the Clavey River drainage above the gaging station. Figure 3 shows in more detail the watershed, the project's points of diversion, and the points of interest evaluated during this analysis. The project is located in Tuolumne County approximately 11 miles northeast of the town of Tuolumne. The application seeks to divert a maximum of 64.5 acre-feet (af) of water for beneficial use when transported by tanker truck to a bottling facility during the season of January 1 to December 31.

3.0 CURRENT WATER RIGHTS, DIVERSIONS AND POINTS OF INTEREST

3.1 Water Rights and Diversions

Figure 5 shows the only two water rights of record in the Hull Creek drainage basin, up stream of the Marco and Polo Creek/Hull Creek confluences. Water right #A020636-01 is active and allows a diversion of 500 gallons per day at the cabin in Fahey Meadow. Water right # A018652-01 located in Hulls Meadow was canceled and is no longer active. The permitted diversion at Fahey Meadow would total 0.38 acre-feet per annum if the entire permitted volume were diverted. However, likely domestic use at the Fahey Meadow cabin is probably much less. Second, because the cabin is only used seasonally from May 1 to October 31.

The U.S. Forest Service also has a reserved right to use water from the Hull Creek watershed; e.g. for the Hull Creek campground use and range cattle allotment needs. These diversions are seasonal from May 1 to October 31. These usages were estimated and the calculations are included in Appendix I. The estimated consumption for these uses totals 1.34 acre feet per year.

It should be noted that all of the uses detailed above do not actually remove water from the Hull Creek watershed and most of the water consumed undoubtedly is returned to ground water within the basin.

Down stream of the Marco and Polo Creek/Hull Creek confluences are three entities with senior water rights, i.e. the Modesto and Turlock Irrigation Districts, and City and County of San Francisco. The Raker Act, respectively, recognized the senior rights of the Districts and established a water right for San Francisco. Additionally, Board ruling D995 deemed the Tuolumne River to be fully appropriated from July 1 to October 31. Therefore, during that timeframe there is no water consider available for appropriation above Lake Don Pedro. As a result of Application No. 31491, these senior water right holders filed protests of the Application to claim their prior rights and ensure those rights shall not be infringed.

Similar protests by the same senior water right holders were filed against this applicant, when applicant of Application No. 29977, dated July 12, 1991. Those protests were resolved by the Applicant entering Agreements first with the Modesto and Turlock Irrigation Districts, dated December 12, 1992; then the City and County of San Francisco, dated February 17, 1995. The foundation of those agreements is the water diverted pursuant to Application No. 29977 during the period the Tuolumne River is fully appropriated shall be replaced with out of basin Stanislaus River water purchased from the Tuolumne Utility District. That water is released upstream of the Lake Don Pedro dam, so there is no net loss of water upstream of said dam.

That same issue, diverting water during the time a system is fully appropriated, was resolved in writing by the City and County of San Francisco with a letter, dated January 31, 2005. As a result of the inclusion of the two conditions within that letter San Francisco and the Districts protest have been dismissed by the Board.

3.2 Proposed Points of Diversion and Points of Interest

Four points of interest (POI) were evaluated in this study. The first POI, labeled "A" on Figures 3, 4 and 6, is the point immediately below the confluence of the unnamed tributary below Marco spring and Hull Creek. The second POI, labeled "B" on Figures 3, 4, & 6, is the point on Hull Creek immediately below the confluence of the unnamed tributary below Polo spring and Hull Creek..

The third POI, labeled "C" on Figures 3. & 4, is the point immediately above the confluence of Hull Creek and the Clavey River. This point of interest measures the effect of the diversions on the entire flow from the Hull Creek watershed.

The fourth location (POI), labeled "D" on Figure 4, is gaging station #11283500, located on the Clavey River below the mouth of Hull Creek. This point of interest measures the effect of the diversions on the flow of the Clavey River below and near the mouth of Hull Creek.

There is no need for any additional POI locations downstream of the Clavey River POI. As explained above, in Section 3.1, the prior rights of the Modesto and Turlock Irrigation Districts, and City and County of San Francisco are protected by the inclusion of two conditions in the Permit to be issued the Applicant. If a potential or actual water supply reduction is determined to or has occurred then upon notice to the Applicant by the Districts replacement water shall be introduced above the Lake Don Pedro dam within one year of said notice. The replacement water shall come from, out of basis, the Stanislaus River. Additionally, the Applicant can and has been purchasing out of basin water in advance as a credit to future replacement water requirements.

4.0 METHODS

4.1 Alternatives

Two methods were used to calculate the runoff from the Hull Creek drainage. The method frequently used by the California State Water Resources Control Board is the Rational Runoff Method. Although CalTrans uses this method only to estimate peak flows, the SWRCB adopted a similar approach to estimate average annual runoff volume from a drainage basin. Nevertheless, this method is subject to serious drawbacks as explained below. Nevertheless, this method was used initially because it was believed that no adequate gaging station was present in the area.

The second and preferred method was comparison with the flow rates determined from a stream gaging station on the Clavey River a short distance downstream from the mouth of Hull Creek.

4.2 Rainfall-Runoff Method

Rainfall runoff methods use rainfall data and land use characteristics to calculate runoff for a particular watershed area. When the rate of rainfall exceeds the rate of infiltration of water into the ground, excess water (runoff) is available to supply surface waters. The rational method is typically used by engineers and hydrologists to design hydraulic structures and predict peak flood flows. However, under the assumptions discussed below, the rational method can be used to estimate the average annual runoff based on the average annual precipitation. The equation is shown below:

$$Q = C I A$$

Where: Q = Estimated average annual runoff (acre-feet per annum);
C = Runoff coefficient;
I = Average annual precipitation (feet per annum); and
A = Tributary watershed area (acres)

The runoff coefficient "C" in the rational method equation represents the percent of water that will run off the ground surface during a storm event. The California Department of Transportation (Caltrans) Highway Design Manual provides a table showing various values for "C" depending on soil type, relief, vegetation and surface storage (California Department of Transportation, 1995). Where multiple land uses are found within the watershed, it is customary to use an area-weighted runoff coefficient (Bedient and Huber, 1992). In addition, the runoff coefficients given in the Caltrans Highway Design Manual are applicable for storms of up to 5 or 10-year frequencies. Less frequent, higher intensity storms require adjustment. The model also does not account for the fact that a significant percentage of the rainfall that infiltrates into the ground and ground water appears again as springs that flow back into Hull Creek and contribute to the runoff.

Since the rational method is so commonly used, it is important to note the assumptions in its development. The equation assumes that rainfall is of equal intensity over the entire watershed. Because actual rainfall rates vary over space and time, the rational method should only be used

within small watershed areas where rainfall is likely to be relatively uniform. For estimation of peak flows, the rational method should not be used for areas larger than 0.5~1 mi² (321~640 acres) (Bedient and Huber , 1992; Linsley, et al, 1992). When the rational method is used with larger watersheds, the peak runoff will generally be over-predicted (Linsley, et al, 1992). Larger watersheds that include significant tributary inflows should be divided into smaller areas and modeled using flow routing methods or regional regression equations (Linsley, et al, 1992).

4.3 Proration of U.S.Geological Survey Streamflow Data

Streamflow can also be estimated based on a proration of areas using the following formula:

$$Q_2 = Q_1 \times (A_2/A_1) \times (I_2/I_1)$$

Where: Q_2 = Daily flow (cfs) at point of interest on tributary watershed;

Q_1 = Daily flow (cfs) at nearby gage;

A_2 = Watershed area above point of interest;

A_1 = Watershed area above nearby gage;

I_2 = Precipitation at point of interest; and

I_1 = Precipitation at nearby gage

In the case of Hull Creek, no rainfall data is available except at the Cherry Lake Dam gauge. Therefore, the assumption must be made that precipitation is constant over the entire watershed.

The total average precipitation over a thirty-year period at the Cherry Valley Dam is 47.46 inches, or 3.98 feet (California State Climatologist). The Cherry Valley Dam rainfall recording station is at an elevation of 4765 feet, whereas the elevation of the Hull Creek drainage ranges from a low of 3850 to a high of 6800 feet above mean sea level.

The map of average annual precipitation in northern California from 1961 to 1990 was also reviewed (National Oceanic and Atmospheric Administration, 2010). This map revealed that the average annual precipitation for the Hull Creek and the balance of the Clavey River drainage ranges from 40 to 55 inches (3.33 to 4.58 feet). The distribution of rainfall appears to be approximately the same for the Hull Creek and the balance of the Clavey River watershed.

5.0 ANNUAL UNIMPAIRED FLOW

5.1 Rainfall and Calculation of Watershed Areas

The drainage areas above points of interest A, B, C, & D were determined and outlined on the US Geological 7.5 minute quadrangles covering the area and the relative areas measured by Golden State Surveying & Engineering of Sonora, California, utilizing the AutoCad computer program algorithm for calculating area. The acreage determined for the areas involved are tabulated in Table 1.

Table 1. Watershed Areas Above Points of Interest

Area Determined	Area (Acres)
Hull Creek above Marco Creek (POI A)	8,175
Hull Creek Between Marco and Polo Creeks (POI B)	413
Hull Creek Between Polo Creek And Clavey River (POI C)	987
Total Hull Creek Drainage above Confluence with Clavey River (POI C)	9,574
Clavey River Above Gaging Station #11283500 (Excluding Hull Creek)	41,569
Clavey River Above Gaging Station #11283500 (Including Hull Creek, POI D)	51,143

5.2 Calculation of Runoff Using the Rainfall-Runoff Method

To calculate the average annual runoff from Hull Creek and Clavey River watersheds the average annual precipitation is assumed to be 4.0 feet per year.

Using the above, the Runoff Coefficient was calculated using the California Department of Transportation Table for the Hull Creek drainage area as follows:

Table 2. Tabulation of Characteristics and Determination of Runoff Coefficient of the Hull Creek Watershed

Watershed Characteristic	Description from Table	Runoff Capacity	Range	Value Used
Relief	Hilly, with average slopes of 10 to 30%	High	0.20-0.28	0.28
Soil Infiltration	slow to take up water, clay or shallow loam soils of low infiltration capacity, imperfectly or poorly drained	High	0.08-0.12	0.12
Vegetal Cover	Good to excellent; about 90% of drainage area in good grassland, woodland or equivalent cover.	Low	0.04-0.06	0.06
Surface Storage	Low; well defined system of small drainage ways; no ponds or marshes	High	0.08-0.10	0.10
Total Runoff Determined Coefficient				0.56

Using the formula and figures in Table 1, the average annual runoff of the Hull Creek watershed above POI A (Immediately below inflow of Marco Creek):

$$Q = 4.0 \text{ feet/year} \times 8175 \text{ acres} \times 0.56$$

$$Q = 18,312 \text{ acre-feet/year}$$

The area of the drainage above the second point of interest, B (point immediately below the confluence of Polo and Hull Creeks), is 8,587 acres. Using the above assumptions, the runoff calculated at this point is:

$$Q = 4.0 \text{ feet/year} \times 8,587 \text{ acres} \times 0.56$$

$$Q = 19,234 \text{ acre-feet/year}$$

The area of the drainage above the third point of interest, C (point immediately above the confluence of Hull Creek and Clavey River), is 9,574 acres. Using the above assumptions, the runoff calculated at this point is:

$$Q = 4.0 \text{ feet/year} \times 9,574 \text{ acres} \times 0.56$$

$$Q = 21,446 \text{ acre-feet/year}$$

The area of the drainage above the fourth point of interest, D (point at gaging station #11283500), is 51,143 acres. Using the above assumptions, the runoff calculated at this point is:

$$Q = 4.0 \text{ feet/year} \times 51,143 \text{ acres} \times 0.56$$

$$Q = 114,560 \text{ acre-feet/year}$$

5.3 Calculation of Runoff using USGS Gage Data

In order to calculate the runoff from Hull Creek using nearby stream gage data, a search was made to determine if there were any stream gages in the vicinity that could be used to calculate the Hull Creek runoff. Two gages were identified that were in close proximity to the Hull Creek Drainage. Gage #11278400 is located 11 miles southeast of the mouth of Hull Creek. Gage #11283500 is located on the Clavey River approximately one and one half miles below the mouth of Hull Creek.

Gage 11278400 is located on Cherry Creek below the Dion R. Holm powerhouse. The drainage basin above the gage has an area of 234 mi² and extends eastward into the Emigrant Wilderness and to the crest of the Sierra. Because the drainage basin extends to higher elevations than Hull Creek, the runoff is affected to a greater extent by snow melt than the flow in Hull Creek. This skews the supply season to later than would be the case in Hull Creek. Furthermore, the flows measured at gage 11278400 are believed to be unreliable because the flows are regulated by Cherry Lake, 11 miles upstream, and Lake Eleanor, 10 miles upstream. Also, the flow above the gage is diverted at times into Cherry Creek Canal 2 miles upstream from the gage for domestic use and to supplement flow to Hetch Hetchy Aqueduct.

On the other hand, gage #11283500 is only one and one half miles from the mouth of Hull Creek and the drainage basin above the gage includes runoff from Hull Creek. In addition, the upper reaches of the Clavey River drainage only extend approximately ten miles farther east than that of Hull Creek and 20% of the flow measured by this gage is derived from Hull Creek. The balance of the Clavey drainage would be affected by the same precipitation events and should have a similar monthly runoff signature as that from Hull Creek .

Table 3. Monthly Measurements of Stream Flow In Clavey River Measured By Gage 11283500 Near Buck Meadows, California, Measured for 30 Years During the Period 1960-1995. Source: USGS & Turlock Irrigation District.

Water Year	Oct (ft ³ /sec)	Nov (ft ³ /sec)	Dec (ft ³ /sec)	Jan (ft ³ /sec)	Feb (ft ³ /sec)	Mar (ft ³ /sec)	Apr (ft ³ /sec)	May (ft ³ /sec)	Jun (ft ³ /sec)	Jul (ft ³ /sec)	Aug (ft ³ /sec)	Sep (ft ³ /sec)	Mean Annual Flow (ft ³ /sec)	Annual Volume (acre-ft)
1960	13.9	17.0	36.6	184	351	418	352	83.8	18.2	9.36	7.96	14.9	125	90,496
1961	24.0	44.3	29.0	79.4	113	215	185	63.7	9.62	4.20	4.98	11.2	65.1	47,130
1962	12.3	27.2	28.3	372	201	988	642	360	53.3	16.0	9.92	6.07	224	162,169
1963	16.2	44.5	245	724	192	610	1034	369	83.9	29.3	19.9	25.0	279	201,988
1964	148	72.2	73.7	111	156	379	403	191	35.5	13.7	10.7	22.3	134	97,012
1965	57.7	999	617	442	375	745	777	449	122	71.4	24.8	10.6	391	283,072
1966	226	141	129	133	385	551	305	61.6	18.5	10.0	8.96	19.4	165	119,455
1967	102	427	195	317	734	471	1548	1005	296	53.2	30.6	9.14	434	314,203
1968	25.4	46.2	69.1	276	281	397	291	80.1	17.4	11.8	6.92	24.7	126	91,220
1969	94.5	101	1302	483	497	1362	1703	769	202	38.5	22.7	13.9	549	397,460
1970	48.7	207	1070	414	466	380	504	239	50.6	17.6	14.3	45.7	288	208,503
1971	124	176	202	276	443	575	584	359	68.2	18.8	14.0	15.7	237	171,581
1972	62.2	139	110	189	490	405	405	143	21.8	9.65	7.96	17.3	167	120,903
1973	35.6	127	253	304	338	799	1163	336	44.5	18.5	13.5	13.0	287	207,779
1974	277	246	438	205	627	765	873	299	75.0	26.1	12.9	23.4	323	233,842
1975	29.0	62.0	94.0	216	439	446	1448	813	130	42.5	26.8	18.6	314	227,327
1976	81.1	51.0	41.6	70.0	135	187	195	34.5	10.2	17.6	12.4	86.9	76.9	55,673
1977	12.6	9.65	17.2	30.0	39.0	84.4	117	43.5	5.06	1.66	2.28	10.6	31.0	22,443
1978	11.4	111	285	452	916	993	1201	732	161	28.5	68.3	2.89	413	299,000
1979	30.4	47.2	214	216	515	810	1116	277	52.0	22.9	16.2	20.3	278	201,264
1980	51.4	71.0	1331	1156	575	821	926	549	200	38.1	23.3	23.9	478	346,058
1981	21.4	33.6	59.0	120	213	460	358	79.8	15.6	7.45	6.77	20.5	116	83,981
1982	295	510	394	1426	714	2057	1231	409	168	57.6	69.4	28.5	606	438,726
1983	339	747	527	824	1482	888	1754	1746	566	101	57.2	226	771	558,181
1987	19.5	21.2	29.0	76.6	165	282	160	30.2	9.60	5.02	4.99	23.5	68.7	49,737
1988	22.7	41.4	88.5	125	209	226	187	57.9	12.8	3.98	3.12	9.13	82.0	59,365
1992	15.3	31.2	24.8	35.4	172	284	415	138	27.0	48.9	8.51	4.57	50.4	36,509
1993	9.62	21.9	60.5	456	376	902	1009	1092	530	122	23.0	12.7	193.9	140,379
1994	15.2	16.6	23.1	28.4	64.5	215	291	290	64.6	11.6	4.06	3.81	43.2	31,282
1995	13.5	57.7	69.2	696	434	1446	1097	no data						
Mean	74.5	154.9	268.5	347.9	403.2	638.7	742.5	382.8	105.8	29.5	18.5	26.4	266.1	191,621
Monthly Percentage	2.33	4.85	8.41	10.90	12.63	20.00	23.25	12.00	3.31	0.92	0.58	0.83	100.01	

Assuming similar precipitation over the Clavey and Hull Creek watersheds, the average annual runoff at Point of interest A can be calculated by the formula:

$$Q_2 = Q_1 \times (A_2/A_1)$$

Where: Q_1 = Measured average annual runoff from Clavey River watershed, including Hull Creek
(=191,621 acre-feet)

A_2 = Area of Hull Creek Drainage Above POI A
(=8,174 acres/640=12.77 mi²)

A_2 = Area of Clavey River Drainage above gage #11283500 (includes Hull Creek)
(=51,143, or 79.91 mi²)

Q_2 = Runoff in Hull Creek at POI A

Substituting:
 $Q_2 = 12.77 \text{ mi}^2 / 79.9 \text{ mi}^2 \times 191,621 \text{ acre-feet}$

$$Q_2 = 30,626 \text{ acre-feet}$$

Again assuming similar precipitation over the Clavey and Hull Creek watersheds, the average annual runoff at Point of interest B can be calculated by the formula:

$$Q_2 = Q_1 \times (A_2/A_1)$$

Where: Q_1 = Measured average annual runoff from Clavey River watershed, including Hull Creek
(=191,621 acre-feet)

A_2 = Area of Hull Creek Drainage Above POI B
(=8,588 acres/640=13.42 mi²)

A_2 = Area of Clavey River Drainage, including Hull Creek
(=79.91 mi²)

Q_2 = Runoff in Hull Creek at POI B

Substituting:
 $Q_2 = 13.42 \text{ mi}^2 / 79.91 \text{ mi}^2 \times 191,621 \text{ acre-feet}$

$$Q_2 = 32,181 \text{ acre-feet}$$

Again assuming similar precipitation over the Clavey and Hull Creek watersheds, the average annual runoff at Point of interest C can be calculated by the formula:

$$Q_2 = Q_1 \times (A_2/A_1)$$

Where:

Q_1 = Measured average annual runoff from Clavey River watershed, including Hull Creek
 $(=191,621 \text{ acre-feet})$

A_2 = Area of Hull Creek Drainage Above POI C
 $(=9574 \text{ acres}/640=14.96 \text{ mi}^2)$

A_2 = Area of Clavey River Drainage above gage #11283500, including Hull Creek
 $(=79.91 \text{ mi}^2)$

Q_2 = Runoff in Hull Creek at POI C

Substituting:

$$Q_2 = 14.96 \text{ mi}^2/79.91 \text{ mi}^2 \times 191,621 \text{ acre-feet}$$

$$Q_2 = 35,874 \text{ acre-feet}$$

5.4 Comparison of Flow Rates

The comparison of flow determined for the points of interest by means of the rational runoff method and calculated total annual flow determined by prorating acreages are tabulated in Table 4.

Table 4. Comparison of Total Flow Determinations

Point of Interest	Mean Flow Rate by Rational Runoff Method (acre-feet/year)	Mean Flow Rate by Gage #11283500 And Prorated Acreages (acre-feet/year)
A	18,312	30,626
B	19,234	32,181
C	21,446	35,874
C	114,560	191,621*

*Mean Measured Flow at Gage #11283500

The table shows a 40% decrease in calculated flow using the rational runoff method when compared to the actual flow data from gage #11283500. The upper reaches of the Clavey drainage have areas that are near or above the tree line and would have a higher runoff coefficient than assumed in Table 2. However, this discrepancy may be greater than can be accounted by an error in the runoff coefficient alone. It is also possible that the upper portion of the Clavey receives greater annual precipitation than determined by the Cherry Dam rain gauge or estimated by the NOAA precipitation map.

Because the Hull Creek drainage is at a lower elevation than the rest of the Clavey drainage basin, it was decided to use the values determined using the rational runoff method for points of interest A, B & C. However, the actual mean runoff figure for gage #11283500 was used for point of interest D. The monthly percentages of runoff at the gage were applied to the flow rates determined by the rational runoff method for Hull Creek.

6.0 UNIMPAIRED FLOW DURING THE PROJECT'S DIVERSION SEASON

6.1 Data and Assumptions

Sum of daily flows were calculated on a percentage basis by comparison of the average annual runoff to the percentage of flows occurring during this time in the closest reliable stream gage. However, the Clavey River, into which Hull Creek flows, has no diversions. A gage on the Clavey, located approximately one mile below the mouth of Hull Creek is currently inactive. However, this gage (#11283500) was monitored by the USGS from 1960 until 1988. The gage was then maintained and monitored by the Turlock Irrigation District until September 1995. This gage is located at latitude 37°54'02" and longitude 120°04'15".

6.2 Calculations

Because diversions from the springs are expected to take place during the entire year, a calculation was made to estimate the average flow for each month of the year. The mean daily flows from gage 11283500 for the period from 1960 to 1995 were converted to acre-feet per month by the following formula:

$$V = f \times d \times s \times g / v$$

where: V = acre feet/month
and, f = daily flow (cubic feet/second)
 d = days per given month
 s = seconds/day
 g = gallons/cubic foot
 v = gallons/acre-foot

The percentage volume for each month was then calculated by dividing the volume for any given month by the total annual volume. This percentage is applied to the annual unimpaired flow calculated for each of the points of interest in the Hull Creek drainage. The results are tabulated in Table 5:

Table 5. Calculated Unimpaired Flow Volumes at Points of Interest A, B, C, & D.

Month	Mean Daily flow from 11283500 (ft ³ /sec)	Mean Volume per Month at 11283500 (acre-feet)	Monthly Percentage of Annual Flow	Calculated Monthly Unimpaired Runoff POI A (acre-feet)	Calculated Mean Daily flow for POI A (ft ³ /sec)	Calculated Monthly Unimpaired Runoff POI B (acre-feet)	Calculated Mean Daily flow for POI B (ft ³ /sec)	Recorded Monthly Unimpaired Runoff POI C (acre-feet)	Recorded Mean Daily flow for POI C (ft ³ /sec)	Recorded Monthly Unimpaired Runoff POI D (acre-feet)	Recorded Mean Daily flow for POI D (ft ³ /sec)
October	74.5	4,281	2.23	408	7.1	429	7.5	478	8.3	4,281	74.5
November	154.9	9,218	4.81	881	14.8	925	15.5	1,031	17.3	9,218	154.9
December	268.5	16,511	8.62	1,578	25.7	1,658	27.0	1,849	30.1	16,511	268.5
January	347.9	21,394	11.16	2,044	33.2	2,147	34.9	2,393	38.9	21,394	347.9
February	403.2	22,395	11.69	2,141	38.5	2,248	40.5	2,507	45.1	22,395	403.2
March	638.7	39,277	20.50	3,754	61.0	3,943	64.1	4,396	71.5	39,277	638.7
April	742.5	44,187	23.06	4,223	71.0	4,435	74.5	4,945	83.1	44,187	742.5
May	382.8	23,540	12.28	2,249	36.6	2,362	38.4	2,634	42.8	23,540	382.8
June	105.8	6,296	3.29	602	10.1	633	10.6	706	11.9	6,296	105.8
July	29.5	1,814	0.95	174	2.8	183	3.0	204	3.3	1,814	29.5
August	18.5	1,137	0.59	108	1.8	113	1.8	127	2.1	1,137	18.5
September	26.4	1,571	0.82	150	2.5	158	2.7	175	3.0	1,571	26.4
Yearly Average											
Total		191,621	100.00	18,312		19,234		21446		191,621	

7.0 BYPASS FLOW

In California basins dominated by rainfall runoff and flowing unimpeded to the Pacific Ocean, bypass flow is normally calculated on the basis of the February median flow. The February median flow metric is accepted as the critical flow level which must be maintained or exceeded in these rivers. This flow is provided in an effort to ensure salmon and steelhead can spawn, their resulting fry are able to thrive, and as fingerlings can be assisted on their return to the sea by the flushing effect of the respective flow metric.

However, this project is located in a drainage basin which is dominated by snowmelt runoff that is impeded from flowing to the sea by New Don Pedro Reservoir. Salmon and steelhead cannot pass the dam that creates New Don Pedro Reservoir and spawn upstream from the dam. Additionally, the applicant is obligated to replace the water diverted upstream of New Don Pedro with out-of-basin waters. This project will have no impact on water quantity or quality downstream from the New Don Pedro Reservoir. As a result, there will be no impact to the bypass flow measurement prescribed for the Tuolumne River downstream of New Don Pedro Dam.

From previous studies by Halstead & Associates (December 2003): "The downstream reaches of Deadwood Creek have not been impacted by the water diversion because of tributary inflows from other springs and creeks." Of the downstream water courses that have had their spring-headwaters diverted by the applicant (Application No. 29977, Water Rights Permit 20784); no correlation has been found to suggest the amount of water, in question, when diverted, has any impact on the quantity or quality of flow along the downstream reaches of a spring's respective stream. The quantity and quality flow parameters were found to be more closely correlated and proportional to the percentage of normal annual rainfall received during that water-year. After being studied during a series of diversion-years, none of the downstream reaches were considered to have less ecological vigor than existed prior to diversion.

As stated by the Dept. of Fish & Game, Stream Alteration Agreement (SAA) No. 4-146-91, Provision 2, bypass flow "is expected to support aquatic life and to maintain in a live healthy condition, the riparian vegetation growing in the reach of the stream that lies" beneath the spring(s). The rate of flow prescribed in aforementioned SAA by the Fish & Game to accomplish that goal was "not less than 2.5 GPM or 20% of the total flow for the spring(s), whichever is greater." The SAA above governs the diversion of water from springs at the same elevation and within two (2) mile of the Marco and Polo springs.

The Fish & Game bypass flow expectation to achieve their stated goal shall be used to set the minimum bypass flow level, surface flow in excess of that amount but no greater than 20 GPM, may be considered available for diversion.

Total Flows	By Pass Flow	Diversion Flow Available
0.0 – 2.5 GPM	0 - 2.5 GPM	0.0
2.5 – 12.5 GPM	2.5 GPM	0.01 – 10.0 GPM
12.5 – 25 GPM	2.5 - 5 GPM	10.01 – 20.0 GPM
> 25 GPM	> 5 GPM	20 GPM

7.2 Water Rights

Down stream of the Marco and Polo Creek/Hull Creek confluences are three (3) entities with senior water rights, i.e. the Modesto and Turlock Irrigation Districts, and City and County of San Francisco. The Raker Act, respectively, recognized the senior rights of the Districts and established a water right for San Francisco. As a result, Board ruling D995 deemed the Tuolumne River to be fully appropriated from July 1 to October 31. During that timeframe there is no water consider available for appropriation above Lake Don Pedro., Therefore, these senior water right holders filed protests to claim their prior rights and ensure those rights shall not be infringed upon by Application No. 31491.

Similar protests by the same senior water right holders were filed against this Applicant, when applicant of Application No. 29977, dated July 12, 1991. Those protests were resolved by the then applicant entering Agreements: first, with the Modesto and Turlock Irrigation Districts, dated December 12, 1992; then the City and County of San Francisco, dated February 17, 1995. The foundation of those agreements is the water diverted pursuant to Application No. 29977 during the period the Tuolumne River is fully appropriated shall be replaced with out of basin Stanislaus River water, purchased from the Tuolumne Utility District. That water is released into Sullivan Creek thence Lake Don Pedro upstream of the Lake Don Pedro dam, thereby the fully appropriated Tuolumne River has no net loss of water in upstream of said dam.

That same issue, diverting water from the Tuolumne River system during the time period its waters are fully appropriated, was resolved in writing by the City and County of San Francisco with a letter, dated January 31, 2005. That letter requires the inclusion of two (2) detailed conditions; thereby, with those conditions incorporated within the Applicant's Permit, once issued, the Board shall dismissed San Francisco's and the Districts' protest.

7.3 Public Interest

In the public interest of City and County of San Francisco, the Raker Act established a Tuolumne River water right for San Francisco. That Act and right permits San Francisco to convey water from the Tuolumne River to San Francisco to meet its domestic water needs. With the dismissal of San Francisco's protest, as described above in Section 7.2, the public interest of San Francisco's domestic water supply has been protected.

8.0 CUMULATIVE FLOW IMPAIRMENT INDEX (CFII)

Pursuant to CEQA, CESA and ESA, the Division is required to evaluate cumulative impacts to natural hydrology. The CFII is an index that is used to evaluate the cumulative flow impairment demand of all existing and pending projects in a watershed of interest. The CFII is a percentage obtained by dividing **Demand** in acre-feet by **Supply** in acre-feet at a specified **POI**, and for a specified time period, where:

Demand is the “face” value entitlements of all existing and pending water rights, under all bases of right, above the POI in acre-feet, using the Division’s Water Rights Information Management System (WRIMS) database and water right files. Demand includes existing and pending water right applications for “Post-1914” appropriators, Statements of Water Diversion and Use for “Riparian” and “Pre-1914” appropriators, small domestic use registrations, stock pond registrations, and any other known authorized diversions; and

Supply is the seasonal average unimpaired flow above the POI in acre-feet. For the “coastal” watersheds in the counties of Mendocino, Sonoma, Marin and Napa the season of December 15 through March 31 is used to compute supply.

Based on the WRIMS database, as of October 30, 2006, the total entitlements of recorded water rights above the POIs are estimated to be 1.72 acre-feet for POI A; 1.72 acre-feet for POI B; 1.72 acre-feet for POI C, and 1.72 acre-feet for POI D (See Appendices B-D). It was assumed that there were no other pending applications other than the one addressed in this document. Therefore, only one case was prepared for each POI. If the current application is approved, the water rights will increase to 66.22 acre-feet per annum (33.97 af above POI A).

The total annual unimpaired water available at the POIs are estimated to be 18,312 acre-feet at POI A; 19,234 acre-feet at POI B. 21,446 acre-feet at POI C; and 191,621 acre-feet at POI D. The CFII values were estimated as follows:

$$\begin{aligned} \text{CFII @ POI A} &= \text{Demand (af)} \div \text{Supply (af)} \times 100\% = \underline{0.0094\%}; \\ \text{CFII @ POI B} &= \text{Demand (af)} \div \text{Supply (af)} \times 100\% = \underline{0.0089\%}; \\ \text{CFII @ POI C} &= \text{Demand (af)} \div \text{Supply (af)} \times 100\% = \underline{0.0080\%}; \\ \text{CFII @ POI D} &= \text{Demand (af)} \div \text{Supply (af)} \times 100\% = \underline{0.0009\%}; \end{aligned}$$

If the current application is added to the existing water rights, and using the figures from Appendix B, the annual CFII can be calculated as:

$$\begin{aligned} \text{CFII @ POI A} &= \text{Demand (af)} \div \text{Supply (af)} \times 100\% = \underline{0.185\%}; \\ \text{CFII @ POI B} &= \text{Demand (af)} \div \text{Supply (af)} \times 100\% = \underline{0.344\%}; \\ \text{CFII @ POI C} &= \text{Demand (af)} \div \text{Supply (af)} \times 100\% = \underline{0.309\%}; \\ \text{CFII @ POI D} &= \text{Demand (af)} \div \text{Supply (af)} \times 100\% = \underline{0.035\%}; \end{aligned}$$

However, because diversions are proposed during the entire year, monthly calculations for the CII were made, including the current application.

Table 6 CFII calculations and results for POI A (assuming current application is approved)

Month	Demand (acre-feet)	Supply (acre-feet) (From Table 5)	Calculation	CFII Percentage
October	2.83	408	Demand/Supply X 100	0.69
November	2.83	881	Demand/Supply X 100	0.32
December	2.83	1,578	Demand/Supply X 100	0.18
January	2.83	2,044	Demand/Supply X 100	0.14
February	2.83	2,141	Demand/Supply X 100	0.13
March	2.83	3,754	Demand/Supply X 100	0.075
April	2.83	4,223	Demand/Supply X 100	0.067
May	2.83	2,249	Demand/Supply X 100	0.13
June	2.83	602	Demand/Supply X 100	0.47
July	2.83	174	Demand/Supply X 100	1.63
August	2.83	108	Demand/Supply X 100	2.62
September	2.83	150	Demand/Supply X 100	1.75

Table 7. CFII calculations and results for POI B (assuming current application is approved)

Month	Demand (acre-feet)	Supply (acre-feet) (From Table 5)	Calculation	CFII Percentage
October	5.52	429	Demand/Supply X 100	1.29
November	5.52	925	Demand/Supply X 100	0.60
December	5.52	1,658	Demand/Supply X 100	0.33
January	5.52	2,147	Demand/Supply X 100	0.26
February	5.52	2,248	Demand/Supply X 100	0.25
March	5.52	3,943	Demand/Supply X 100	0.14
April	5.52	4,455	Demand/Supply X 100	0.12
May	5.52	2,362	Demand/Supply X 100	0.23
June	5.52	633	Demand/Supply X 100	0.87
July	5.52	182	Demand/Supply X 100	3.03
August	5.52	113	Demand/Supply X 100	4.89
September	5.52	158	Demand/Supply X 100	3.49

Table 8. CFII calculations and results for POI C (assuming current application is approved)

Month	Demand (acre-feet)	Supply (acre-feet) (From Table 5)	Calculation	CFII Percentage
October	5.52	478	Demand/Supply X 100	1.15
November	5.52	1032	Demand/Supply X 100	0.53
December	5.52	1849	Demand/Supply X 100	0.30
January	5.52	2393	Demand/Supply X 100	0.23
February	5.52	2507	Demand/Supply X 100	0.22
March	5.52	4396	Demand/Supply X 100	0.12
April	5.52	4945	Demand/Supply X 100	0.11
May	5.52	2634	Demand/Supply X 100	0.21
June	5.52	706	Demand/Supply X 100	0.78
July	5.52	204	Demand/Supply X 100	2.69
August	5.52	127	Demand/Supply X 100	4.32
September	5.52	176	Demand/Supply X 100	3.12

Table 9. CFII calculations and results for POI C (assuming current application is approved)

Month	Demand (acre-feet)	Supply (acre-feet) (From Table 5)	Calculation	CFII Percentage
October	5.52	4,281	Demand/Supply X 100	0.13
November	5.52	9,218	Demand/Supply X 100	0.060
December	5.52	16,511	Demand/Supply X 100	0.033
January	5.52	21,394	Demand/Supply X 100	0.025
February	5.52	22,395	Demand/Supply X 100	0.024
March	5.52	39,277	Demand/Supply X 100	0.014
April	5.52	44,187	Demand/Supply X 100	0.012
May	5.52	23,540	Demand/Supply X 100	0.023
June	5.52	6,296	Demand/Supply X 100	0.087
July	5.52	1,814	Demand/Supply X 100	0.30
August	5.52	1,137	Demand/Supply X 100	0.48
September	5.52	1,571	Demand/Supply X 100	0.35

9.0 Determination of Spring Diversion Flow Availability

9.1 Characteristics and Occurrence

The location of the springs in the area is controlled by major fault structures in the bedrock that provide pathways along which ground water flows in the bedrock and also to the surface to emerge as springs.

The applicant proposes to develop both Marco and Polo springs by means of boreholes that intercept these faults at a depth below the surface before the ascending spring water comes in contact with the surficial soils. This method of development is essential so that the spring water will not contact the soil profile and become contaminated with soil bacteria. During operation of the spring diversion, it is imperative to maintain surface flow from the springs to prevent infiltration of surface water into the diverted flow. This surface water will contain soil bacteria that could contaminate the diverted spring water.

Therefore, since the applicant must maintain surface flow from the springs, this will result in an inundated ecosystem near the spring water orifices. It will also preserve stream flow downstream from the springs.

9.2 Spring Flow Rates

G. Scott Fahey, a Registered Professional Engineer in the state of Idaho (#5763), measured the flows at two locations below each spring orifice area from 2005 to 2007 (Appendix H). The first site at each spring was immediately below the proposed points of diversion for each spring and the second two sites were where the gulches below the spring crossed the old railroad grade (Figure 6).

The flows measured at Marco and Polo springs were compared to those at Deadwood and Sugar Pine springs that have been continuously monitored from May of 2005 to June of 2008 (Figure 8).

In order to measure the flow, dams were built across the spring flow at each site and a four-inch PVC pipe was inserted in each dam. Flows less than approximately 100 gallons per minute were measured by Mr. Fahey by means of a five gallon bucket and stopwatch. Flows greater than 100 gallons per minute were estimated. The flow rates measured from each of the four sites are tabulated in Appendix H. As can be seen from the tabulation, the flow increases significantly below the proposed point of diversion to the railroad grade sites. This demonstrates that the streams continue to gain spring flow between the proposed point of diversion and the railroad grade.

The closest rainfall gauge at a similar elevation, the Cherry Valley Dam gauge, has averaged 47.65 inches per season over the last 45 years (<http://www.wrcc.dri.edu/cgi-bin/cliMAIN.pl/ca1697>). The 2004-2005 season at this gauge recorded 68.19 inches of precipitation, 43% above average. The 2005-2006 precipitation season recorded 67.34 inches,

41% above normal. However, the 2006-2007 season only recorded 28.18 inches, 41% below normal.

It is worthy to note that from 1955 to 2007 the seasonal precipitation at the Cherry Valley Dam gauge has ranged from a low of 19.16 inches to a high of 91.03 inches. However only five of the fifty-one complete seasonal records had precipitation totals less than the 2006-2007 season.

Figure 7 shows the normal distribution of this precipitation. Very little rainfall is recorded during the summer with the bulk of the precipitation occurring from November through April.

Table 10 demonstrates the diminution of flows from the springs at the end of the dry season before rain and snowfall replenishes the aquifer. It also shows the relative effects of total annual rainfall on the flows from both Marco and Polo springs.

In order to ensure that surface spring flows are sustained, the proposed diversion flow must be reduced, if necessary, to ensure that surface flow is maintained at 2.5 GPM, or 20% of the total flow, whichever is greater. That minimum stream flow shall be maintained in each stream immediately below each point of diversion. If needed to assure continues stream flow continuity, additional diversion reduction shall occur, so in each spring's stream where they cross the railroad grade below the point of diversion a minimum flow of five gallons per minute shall be maintained.

Table 10 demonstrates the net effect of the diversions at the respective gauging sites if the diversions are maintained to permit the greater of 2.5 GPM or 20% of the total flow is bypassed at the points of diversion and a flow of five gallons per minute at the railroad grade stream crossings.

Table 10. Flow Rates in Marco and Polo Springs if Diversions Occurred During the Historical Periods of Measurement

					Total Flows	By Pass Flow	Diverion Flow Available						
					0.0 – 2.5 GPM	0 - 2.5 GPM	0						
					2.5 – 12.5 GPM	2.5 GPM	0.01 – 10.0 GPM						
					12.5 – 25 GPM	2.5 - 5 GPM	10.01 – 20.0 GPM						
	Deadwood &				> 25 GPM	> 5 GPM	20 GPM						
	Sugar Pine	% of		Polo				% of		Marco			
Date	Total Flow	% Change	DW & SP	Total Flow	Diversion	Bypass Flow		% Change	DW & SP	Total Flow	Diversion	Bypass Flow	
5/26/2005	80.41		174%	70.00	20.00	50.00		199%	80.00	20.00	60.00		
6/2/2005	79.45	1%	173%	68.79	20.00	48.79		0%	199%	78.95	20.00	58.95	
6/7/2005	77.12	1%	172%	66.41	20.00	46.41		0%	199%	76.55	20.00	56.55	
6/16/2005	73.43	1%	171%	62.88	20.00	42.88		0%	198%	72.80	20.00	52.80	
6/23/2005	71.33	1%	170%	60.74	20.00	40.74		0%	198%	70.63	20.00	50.63	
7/1/2005	68.93	1%	169%	58.37	20.00	38.37		0%	198%	68.17	20.00	48.17	
7/7/2005	66.83	1%	168%	56.27	20.00	36.27		0%	198%	66.01	20.00	46.01	
7/10/2005	65.88	1%	167%	55.16	20.00	35.16		0%	197%	65.00	20.00	45.00	
7/15/2005	64.88	1%	166%	54.01	20.00	34.01		0%	197%	63.93	20.00	43.93	
7/20/2005	63.03	1%	165%	52.17	20.00	32.17		0%	197%	62.04	20.00	42.04	
7/22/2005	62.84	1%	165%	51.71	20.00	31.71		0%	197%	61.77	20.00	41.77	
7/29/2005	61.11		164%	50.00	20.00	30.00		196%	60.00	20.00	40.00		
8/3/2005	60.37	3%	160%	48.42	20.00	28.42		-2%	198%	59.78	20.00	39.78	
8/10/2005	59.39	3%	157%	46.67	20.00	26.67		-2%	200%	59.31	20.00	39.31	
8/12/2005	58.90	3%	154%	45.34	20.00	25.34		-2%	201%	59.31	20.00	39.31	
8/18/2005	57.46	3%	151%	43.30	20.00	23.30		-2%	203%	58.34	20.00	38.34	
8/24/2005	56.97	3%	147%	42.01	20.00	22.01		-2%	205%	58.32	20.00	38.32	
9/2/2005	55.66	3%	144%	40.15	20.00	20.15		-2%	206%	57.45	20.00	37.45	
9/8/2005	54.00	3%	141%	38.08	20.00	18.08		-2%	208%	56.19	20.00	36.19	
9/15/2005	53.37	3%	138%	36.77	20.00	16.77		-2%	210%	55.97	20.00	35.97	

Table 10. Flow Rates in Marco and Polo Springs if Diversions Occurred During the Historical Periods of Measurement

					Total Flows	By Pass Flow	Diversion Flow Available					
					0.0 – 2.5 GPM	0 - 2.5 GPM	0					
					2.5 – 12.5 GPM	2.5 GPM	0.01 – 10.0 GPM					
					12.5 – 25 GPM	2.5 - 5 GPM	10.01 – 20.0 GPM					
	Deadwood &				> 25 GPM	> 5 GPM	20 GPM					
	Sugar Pine	% of		Polo				% of		Marco		
Date	Total Flow	% Change	DW & SP	Total Flow	Diversion	Bypass Flow		% Change	DW & SP	Total Flow	Diversion	Bypass Flow
9/28/2005	52.02		135%	35.00	20.00	15.00			211%	55.00	20.00	35.00
10/6/2005	51.19	1%	136%	34.80	20.00	14.80		1%	212%	54.28	20.00	34.28
10/14/2005	50.11	1%	137%	34.41	20.00	14.41		1%	213%	53.28	20.00	33.28
10/17/2005	48.66	1%	139%	33.75	20.00	13.75		1%	213%	51.88	20.00	31.88
10/25/2005	48.19	1%	140%	33.76	20.00	13.76		1%	214%	51.53	20.00	31.53
11/6/2005	48.21	1%	141%	34.11	20.00	14.11		1%	214%	51.70	20.00	31.70
11/12/2005	48.36	1%	143%	34.55	20.00	14.55		1%	215%	52.01	20.00	32.01
12/12/2005	48.20	1%	144%	34.77	20.00	14.77		1%	216%	51.97	20.00	31.97
12/19/2005	47.02	1%	146%	34.25	20.00	14.25		1%	216%	50.85	20.00	30.85
12/23/2005	50.51	1%	147%	37.14	20.00	17.14		1%	217%	54.77	20.00	34.77
12/31/2005	59.28	1%	148%	44.00	20.00	24.00		1%	217%	64.46	20.00	44.46
1/3/2006	64.63	1%	150%	48.42	20.00	28.42		1%	218%	70.48	20.00	50.48
1/5/2006	63.09	1%	151%	47.70	20.00	27.70		1%	219%	68.98	20.00	48.98
1/15/2006	63.68	1%	153%	48.59	20.00	28.59		1%	219%	69.83	20.00	49.83
1/18/2006	62.88	1%	154%	48.41	20.00	28.41		1%	220%	69.13	20.00	49.13
1/22/2006	62.81	1%	155%	48.80	20.00	28.80		1%	221%	69.25	20.00	49.25
1/29/2006	62.14	1%	157%	48.71	20.00	28.71		1%	221%	68.70	20.00	48.70
2/1/2006	62.33	1%	158%	49.29	20.00	29.29		1%	222%	69.10	20.00	49.10
2/10/2006	64.45	1%	160%	51.41	20.00	31.41		1%	222%	71.64	20.00	51.64
2/17/2006	64.26	1%	161%	51.71	20.00	31.71		1%	223%	71.62	20.00	51.62

Table 10. Flow Rates in Marco and Polo Springs if Diversions Occurred During the Historical Periods of Measurement

					Total Flows	By Pass Flow	Diversion Flow Available					
					0.0 – 2.5 GPM	0 - 2.5 GPM	0					
					2.5 – 12.5 GPM	2.5 GPM	0.01 – 10.0 GPM					
					12.5 – 25 GPM	2.5 - 5 GPM	10.01 – 20.0 GPM					
	Deadwood &				> 25 GPM	> 5 GPM	20 GPM					
	Sugar Pine	% of		Polo				% of		Marco		
Date	Total Flow	% Change	DW & SP	Total Flow	Diversion	Bypass Flow		% Change	DW & SP	Total Flow	Diversion	Bypass Flow
2/24/2006	63.16	1%	162%	51.26	20.00	31.26		1%	224%	70.59	20.00	50.59
2/28/2006	63.86	1%	164%	52.27	20.00	32.27		1%	224%	71.56	20.00	51.56
3/1/2006	73.19	1%	165%	60.42	20.00	40.42		1%	225%	82.24	20.00	62.24
3/2/2006	75.07	1%	166%	62.49	20.00	42.49		1%	225%	84.58	20.00	64.58
4/7/2006	75.24		168%	65.00	20.00	45.00			226%	85.00	20.00	65.00
6/5/2006	79.63		138%	55.00	20.00	35.00			163%	65.00	20.00	45.00
8/31/2006	60.00		179%	50.00	20.00	30.00			200%	60.00	20.00	40.00
10/1/2006	52.00		175%	45.00	20.00	25.00			192%	50.00	20.00	30.00
11/30/2006	50.74	4%	172%	43.53	20.00	23.53		-2%	194%	49.28	20.00	29.28
12/25/2006	51.19	4%	168%	42.99	20.00	22.99		-2%	196%	50.22	20.00	30.22
12/31/2006	51.04	4%	164%	41.94	20.00	21.94		-2%	198%	50.57	20.00	30.57
1/7/07	51.12	4%	161%	41.08	20.00	21.08		-2%	200%	51.15	20.00	31.15
2/1/2007	49.10	4%	157%	38.57	20.00	18.57		-2%	202%	49.61	20.00	29.61
2/12/2007	51.30	4%	153%	39.37	20.00	19.37		-2%	204%	52.33	20.00	32.33
2/21/2007	49.31	4%	150%	36.95	20.00	16.95		-2%	206%	50.78	20.00	30.78
3/1/2007	48.61	4%	146%	35.54	20.00	15.54		-2%	208%	50.53	20.00	30.53
3/7/07	48.93	4%	143%	34.89	20.00	14.89		-2%	210%	51.35	20.00	31.35
3/11/07	50.31	4%	139%	34.96	20.00	14.96		-2%	212%	53.28	20.00	33.28
3/18/07	51.20	4%	135%	34.65	20.00	14.65		-2%	214%	54.73	20.00	34.73
4/2/07	53.17	4%	132%	35.02	20.00	15.02		-2%	216%	57.35	20.00	37.35

Table 10. Flow Rates in Marco and Polo Springs if Diversions Occurred During the Historical Periods of Measurement

					Total Flows	By Pass Flow	Diversion Flow Available						
					0.0 – 2.5 GPM	0 - 2.5 GPM	0						
					2.5 – 12.5 GPM	2.5 GPM	0.01 – 10.0 GPM						
					12.5 – 25 GPM	2.5 - 5 GPM	10.01 – 20.0 GPM						
	Deadwood &				> 25 GPM	> 5 GPM	20 GPM						
	Sugar Pine	% of	Polo					% of	Marco				
Date	Total Flow	% Change	DW & SP	Total Flow	Diversion	Bypass Flow		% Change	DW & SP	Total Flow	Diversion		
											Bypass Flow		
4/22/07	51.54	4%	128%	33.01	20.00	13.01		-2%	218%	56.10	20.00	36.10	
5/5/07	50.60	4%	124%	31.50	20.00	11.50		-2%	220%	55.57	20.00	35.57	
5/16/07	49.64		121%	30.00	20.00	10.00			222%	55.00	20.00	35.00	
5/20/07	49.17	4%	117%	28.67	20.00	8.67		9%	212%	52.24	20.00	32.24	
5/23/07	48.80	4%	112%	27.41	20.00	7.41		9%	203%	49.61	20.00	29.61	
6/3/07	47.34	4%	108%	25.59	20.00	5.59		9%	194%	45.97	20.00	25.97	
6/15/07	46.33	4%	104%	24.05	19.24	4.81		9%	185%	42.87	20.00	22.87	
6/30/2007	45.00	4%	100%	22.41	17.92	4.48		9%	176%	39.59	20.00	19.59	
7/12/07	41.96		95%	20.00	16.00	4.00			167%	35.00	20.00	15.00	
8/15/07	37.86	1%	94%	17.78	14.23	3.56		10%	157%	29.72	20.00	9.72	
8/26/07	37.36	1%	93%	17.29	13.83	3.46		10%	147%	27.51	20.00	7.51	
9/10/07	35.16	1%	91%	16.03	12.82	3.21		8%	139%	24.51	19.61	4.90	
10/2/07	34.41	1%	90%	15.45	12.36	3.09		6%	133%	22.90	18.32	4.58	
10/10/07	33.94		88%	15.00	12.00	3.00			118%	20.00	16.00	4.00	
12/12/07	31.39		76%	12.00	9.50	2.5			108%	17.00	13.60	3.40	
12/16/07	31.30	1%	78%	12.18	9.68	2.5		0%	108%	16.90	13.52	3.38	
12/23/07	31.33	1%	79%	12.42	9.92	2.5		0%	108%	16.87	13.50	3.37	
12/31/07	31.21	1%	81%	12.59	10.07	2.52		0%	107%	16.76	13.41	3.35	
1/5/08	31.33	1%	82%	12.86	10.29	2.57		0%	107%	16.78	13.42	3.36	
1/6/08	31.52		1%	83%	13.15	10.52	2.63		0%	107%	16.83	13.46	3.37

Table 10. Flow Rates in Marco and Polo Springs if Diversions Occurred During the Historical Periods of Measurement

					Total Flows	By Pass Flow	Diversion Flow Available				
					0.0 – 2.5 GPM	0 - 2.5 GPM	0				
					2.5 – 12.5 GPM	2.5 GPM	0.01 – 10.0 GPM				
					12.5 – 25 GPM	2.5 - 5 GPM	10.01 – 20.0 GPM				
	Deadwood &				> 25 GPM	> 5 GPM	20 GPM				
	Sugar Pine	% of		Polo				% of		Marco	
Date	Total Flow	% Change	DW & SP	Total Flow	Diversion	Bypass Flow		% Change	DW & SP	Total Flow	Diversion
2/1/08	31.87	1%	85%	13.52	10.82	2.70		0%	106%	16.96	13.57
2/17/08	32.52	1%	86%	14.03	11.22	2.81		0%	106%	17.26	13.81
2/20/08	32.67	1%	88%	14.32	11.46	2.86		0%	106%	17.29	13.83
2/23/08	33.09	1%	89%	14.74	11.79	2.95		0%	106%	17.46	13.97
2/25/08	33.27	1%	90%	15.05	12.04	3.01		0%	105%	17.51	14.01
2/26/08	33.55	1%	92%	15.41	12.33	3.08		0%	105%	17.60	14.08
2/27/08	33.86	1%	93%	15.79	12.63	3.16		0%	105%	17.71	14.17
2/28/08	34.01	1%	95%	16.10	12.88	3.22		0%	104%	17.74	14.19
2/29/08	34.32	1%	96%	16.49	13.19	3.30		0%	104%	17.85	14.28
3/2/08	35.07	1%	97%	17.09	13.67	3.42		0%	104%	18.18	14.55
3/4/08	35.41	1%	99%	17.51	14.01	3.50		0%	103%	18.31	14.64
3/11/08	35.72	1%	100%	17.91	14.33	3.58		0%	103%	18.41	14.73
3/12/08	36.02	1%	102%	18.31	14.65	3.66		0%	103%	18.51	14.81
3/14/08	36.48	1%	103%	18.80	15.04	3.76		0%	102%	18.69	14.95
3/16/08	37.52	1%	104%	19.60	15.68	3.92		0%	102%	19.17	15.33
3/20/08	37.87	1%	106%	20.05	16.04	4.01		0%	102%	19.29	15.43
3/23/08	38.16	1%	107%	20.47	16.38	4.09		0%	102%	19.38	15.50
3/25/08	38.65	1%	109%	21.01	16.81	4.20		0%	101%	19.57	15.65
3/29/08	40.02	1%	110%	22.03	17.63	4.41		0%	101%	20.20	16.16
4/2/08	41.39	1%	111%	23.08	18.46	4.62		0%	101%	20.83	16.66

Table 10. Flow Rates in Marco and Polo Springs if Diversions Occurred During the Historical Periods of Measurement

					Total Flows	By Pass Flow	Diversion Flow Available					
					0.0 – 2.5 GPM	0 - 2.5 GPM	0					
					2.5 – 12.5 GPM	2.5 GPM	0.01 – 10.0 GPM					
					12.5 – 25 GPM	2.5 - 5 GPM	10.01 – 20.0 GPM					
	Deadwood &				> 25 GPM	> 5 GPM	20 GPM					
	Sugar Pine	% of		Polo				% of		Marco		
Date	Total Flow	% Change	DW & SP	Total Flow	Diversion	Bypass Flow		% Change	DW & SP	Total Flow	Diversion	Bypass Flow
4/6/08	41.83	1%	113%	23.62	18.89	4.72		0%	100%	20.98	16.79	4.20
4/8/08	42.17	1%	114%	24.10	19.28	4.82		0%	100%	21.09	16.87	4.22
4/11/08	42.49	1%	116%	24.58	19.66	4.92		0%	100%	21.18	16.95	4.24
4/13/08	42.62	1%	117%	24.95	19.96	4.99		0%	99%	21.18	16.94	4.24
4/20/08	43.12	1%	119%	25.55	20.00	5.55		0%	99%	21.36	17.09	4.27
4/23/08	43.13	1%	120%	25.86	20.00	5.86		0%	99%	21.30	17.04	4.26
4/30/08	43.17	1%	121%	26.18	20.00	6.18		0%	98%	21.26	17.00	4.25
5/18/08	40.75		123%	25.00	20.00	5.00			98%	20.00	16.00	4.00
5/28/08	39.71	-15%	108%	21.49	17.19	4.30		2%	101%	19.99	15.99	4.00
6/8/08	38.75	-15%	94%	18.15	14.52	3.63		2%	103%	19.98	15.98	4.00
6/15/08	37.88		79%	15.00	12.00	3.00			106%	20.00	16.00	4.00

10.0 Conclusions

Marco and Polo springs issue from a series of orifices that are dispersed over an area and flow continues to increase above the old railroad grade.

Flow in Hull Creek, calculated using the rational method, resulted in a much lower volume than that using prorated areas of Hull Creek and the Clavey River and the data from gage #11283500 on the Clavey. The analysis in this report used the lower flow determined by the rational method. However, the higher flow rates measured at the Clavey gage suggest that the flow at the points of interest on Hull Creek may be significantly higher than that used in the analyses. If higher flow rates are used in the analyses, the effect of the proposed diversions would be even less than calculated.

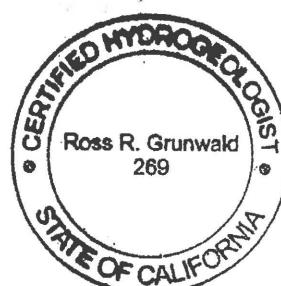
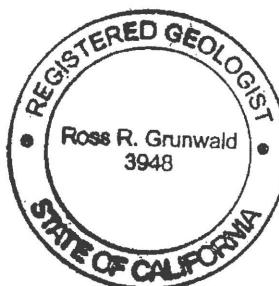
The proposed diversions of water from Marco and Polo Springs would have an insignificant effect on Hull Creek during the supply season of November through June and an insignificant effect on the Clavey River during the entire year. During the late summer and early fall, the diversions could have a greater effect on Hull Creek flow. However, the applicant proposes to maintain a flow of at least 2.5 gallons per minute below each of the spring diversions at all times. Because of the fact that the springs continue to increase in flow below the points of diversions, the flow measured at the old railroad grade will be much greater than 2.5 gallons per minute. The seasonal restriction of diversion during the late summer and fall would result in reduced impact on the flow at the points of interest.

Based on the precipitation and spring flow data it is probable that the proposed diversions of 20 gallons per minute from each spring can be accomplished without restriction during normal and higher than normal rainfall years. During the late summer and early fall of lower than average rainfall seasons, the diverted flow may have to be restricted to maintain flow below the springs.

This report was prepared by:



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FIGURES

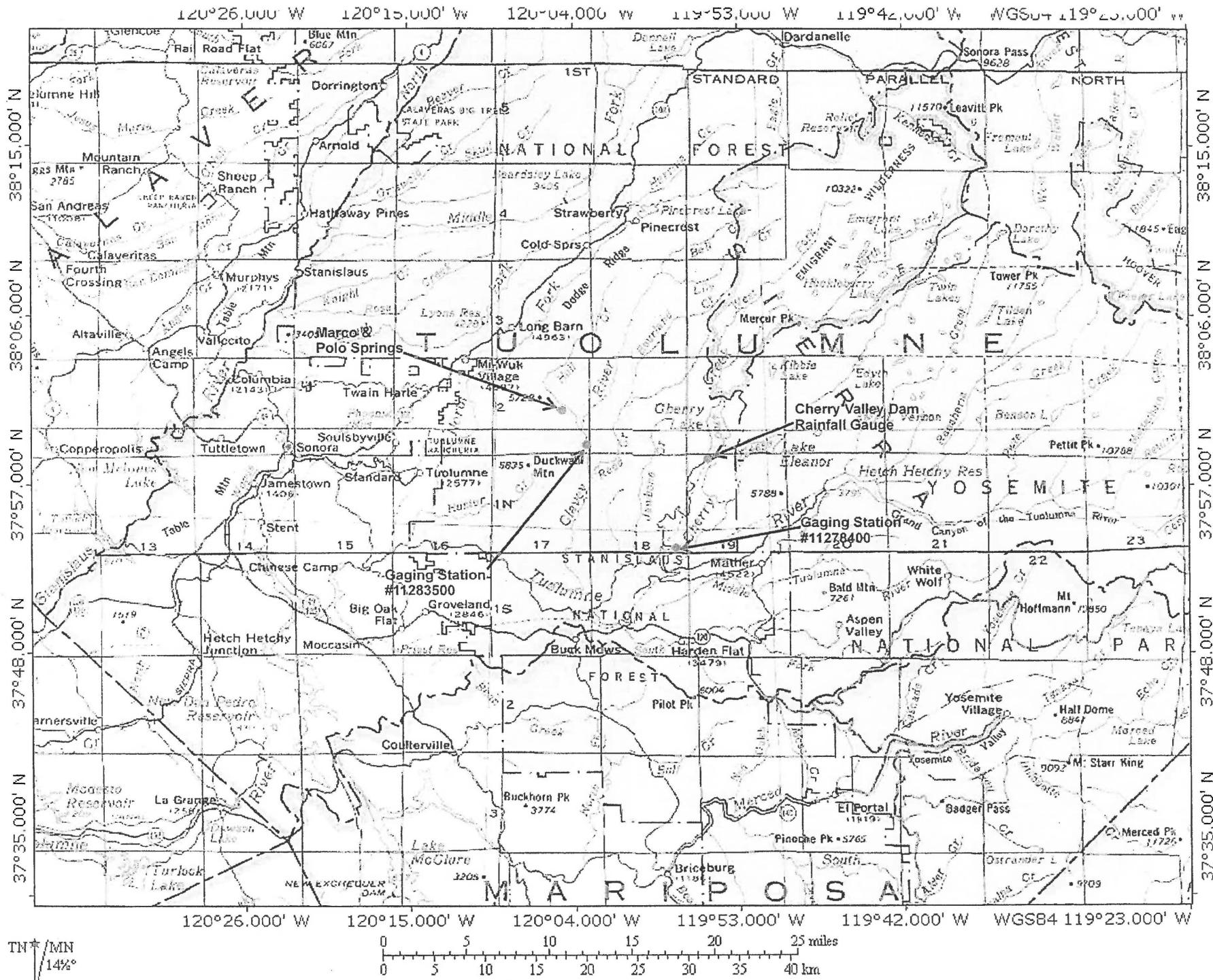


Figure 1. Map showing Location of Marco and Polo Springs,
Cherry Valley Dam Rainfall Gage, and Gaging Stations #11278400 & #11283500

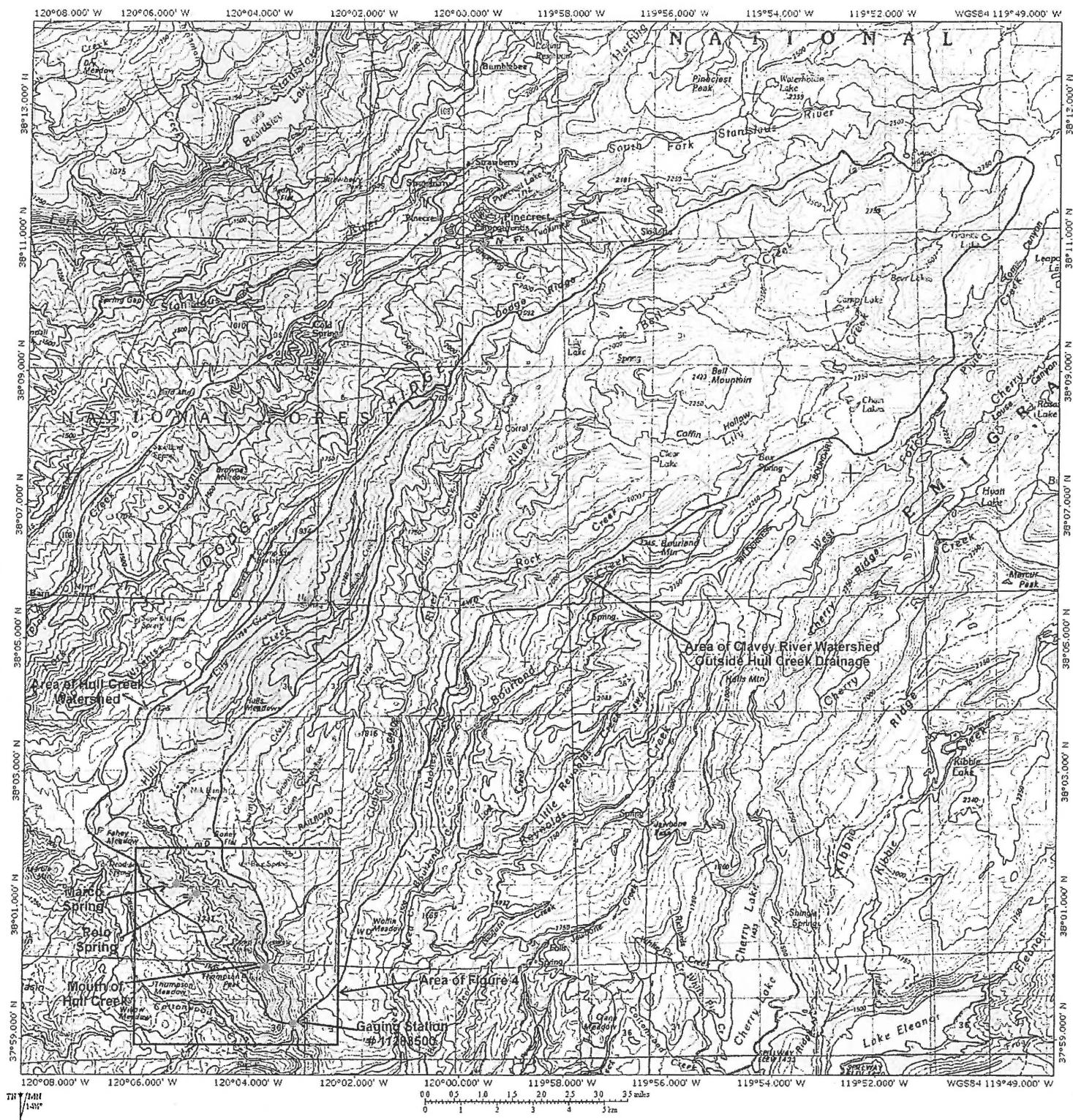


Figure 2. Topographic Map Showing Areas of Clavey and Hull Creek Watersheds,



Figure 3. Topographic Map of Hull Creek showing Watershed, Springs and Points of Interest

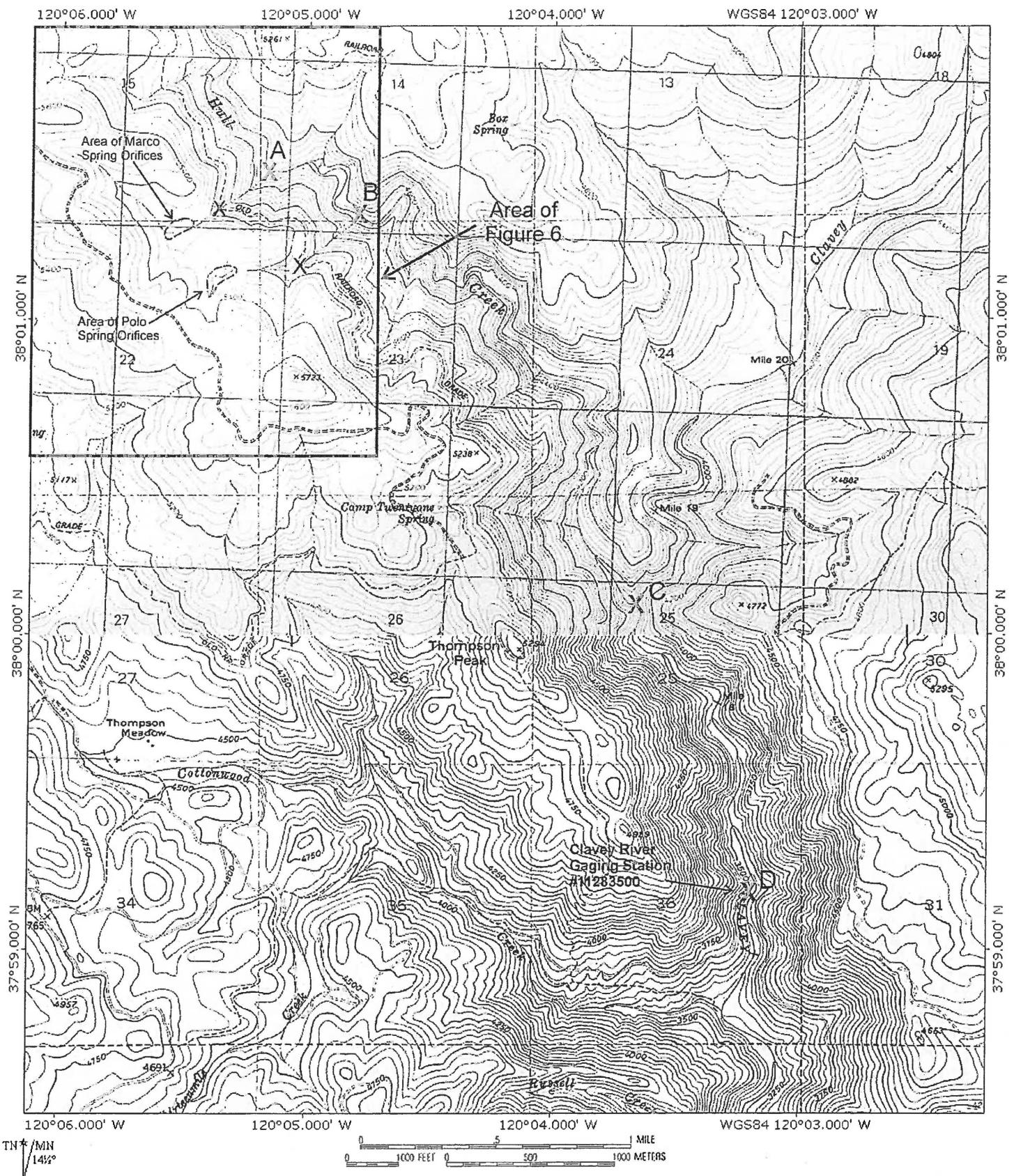


Figure 4. Topographic Map of Marco and Polo Springs and Point of Interest

- X Observation Point on Railroad Grade Below Marco and Polo Springs
- X Points of Interest

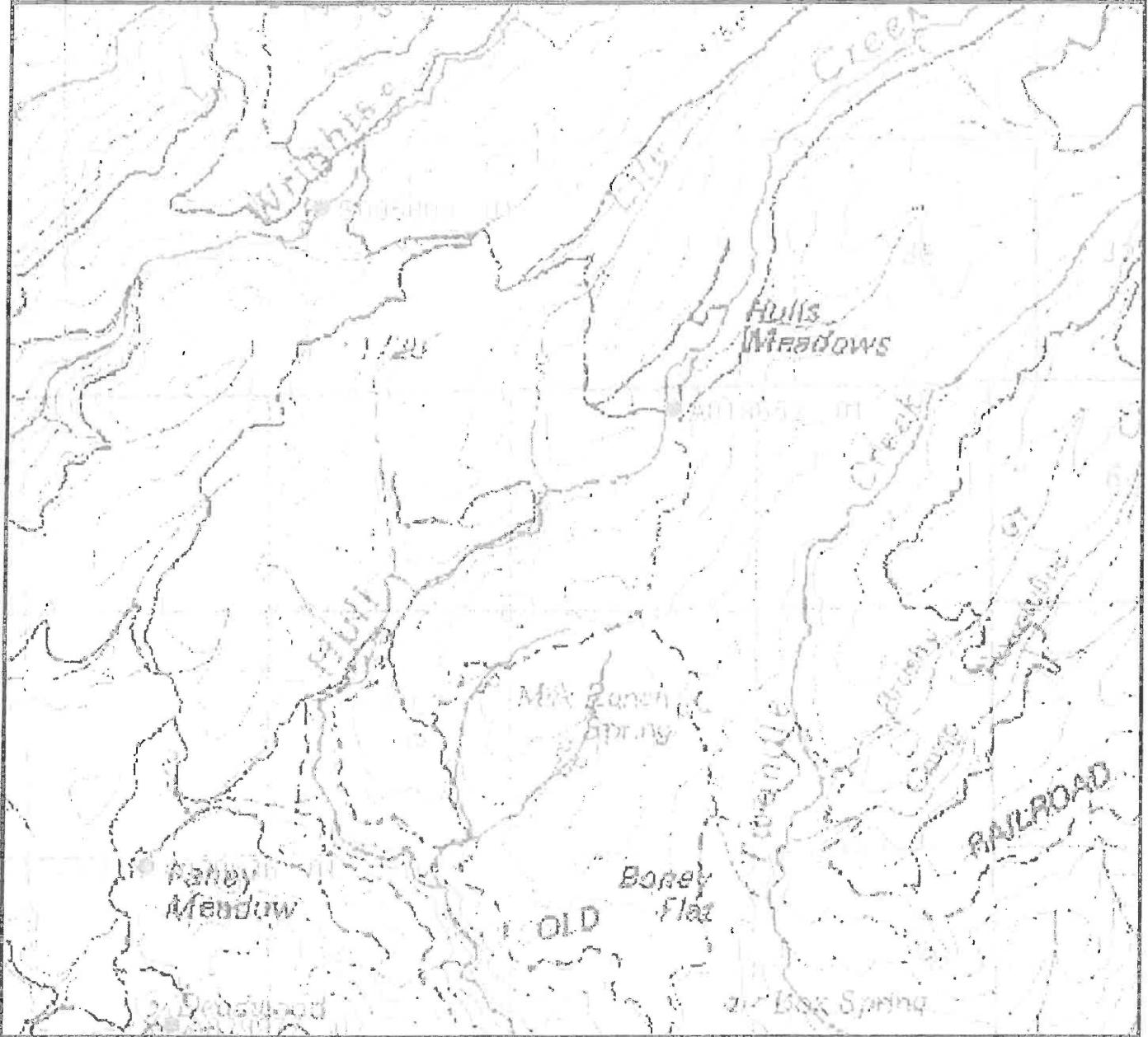


Figure 5. Map of Water Rights of Record in Hull Creek Basin

Water Right:

A018652 01 Cancelled

A020636 01 Fahey Meadow--500 gallons/day

0 1 2 3
MILES



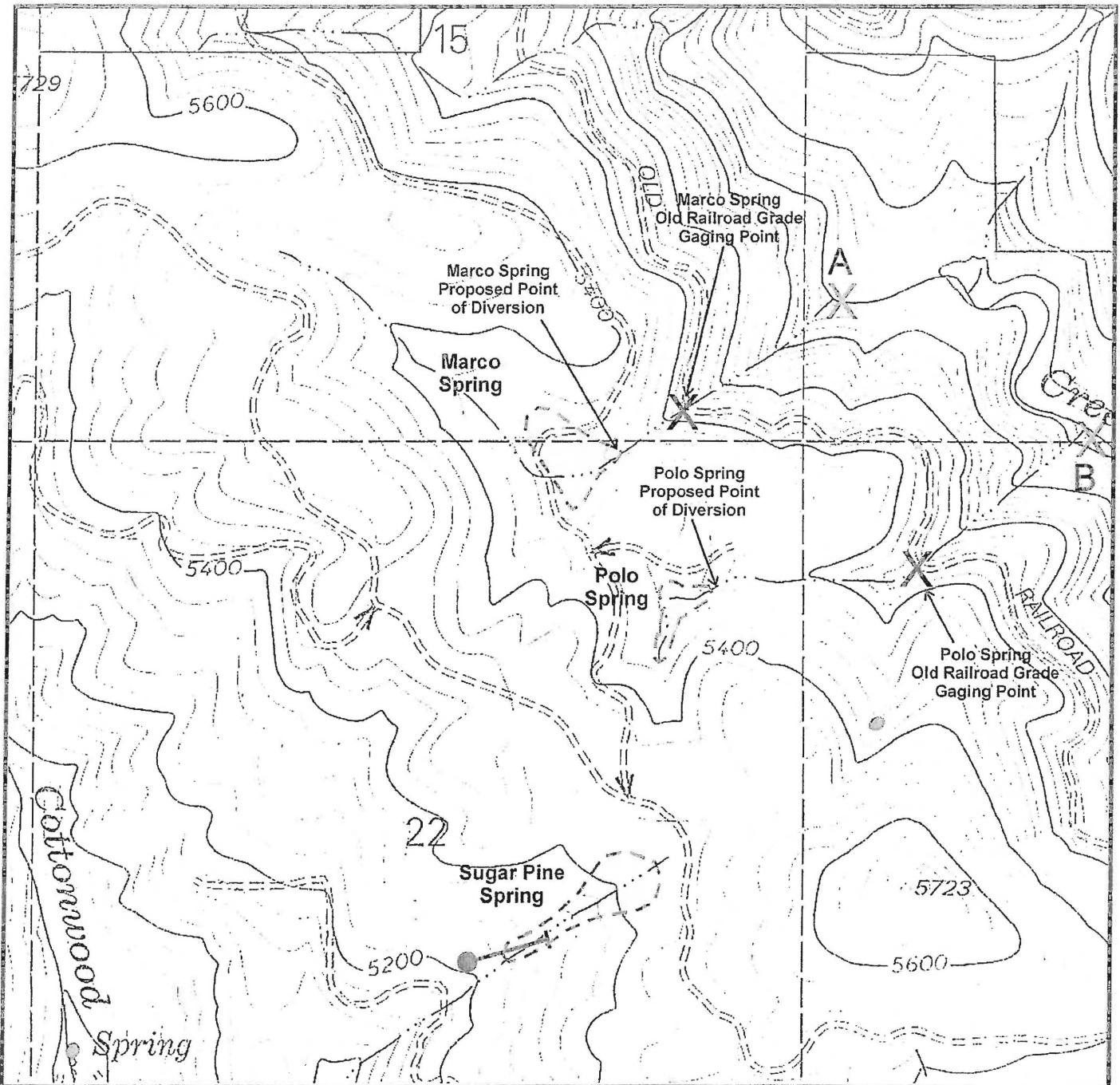
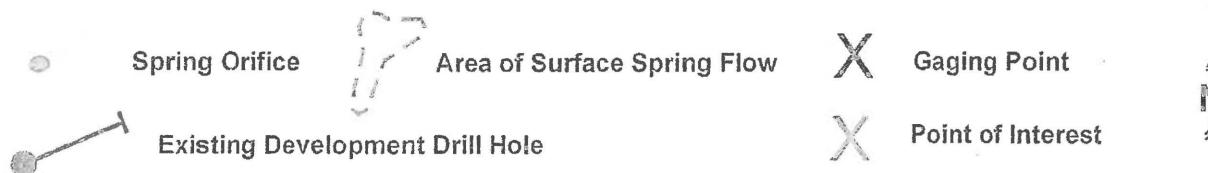


Figure 6. Topographic Map of Project Area showing Springs and Existing Development Drill Hole.

0 1000 2000 3000 4000
FEET



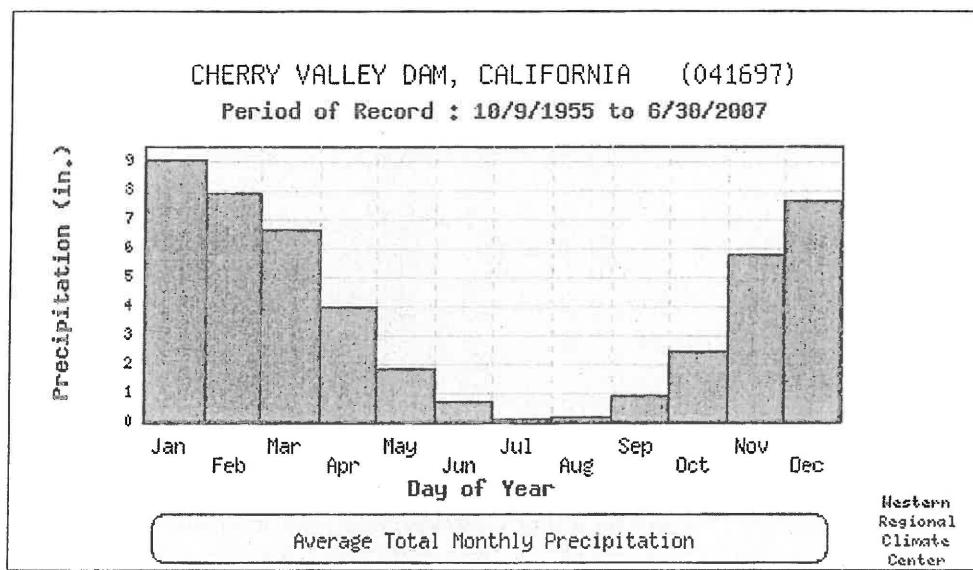


Figure 7. Average Monthly Precipitation for Cherry Valley Dam Rain Gauge

Figure 8. Comparison of Flow Rates for Continuously Monitored Sugar Pine and Deadwood Spring with Marco and Polo Springs

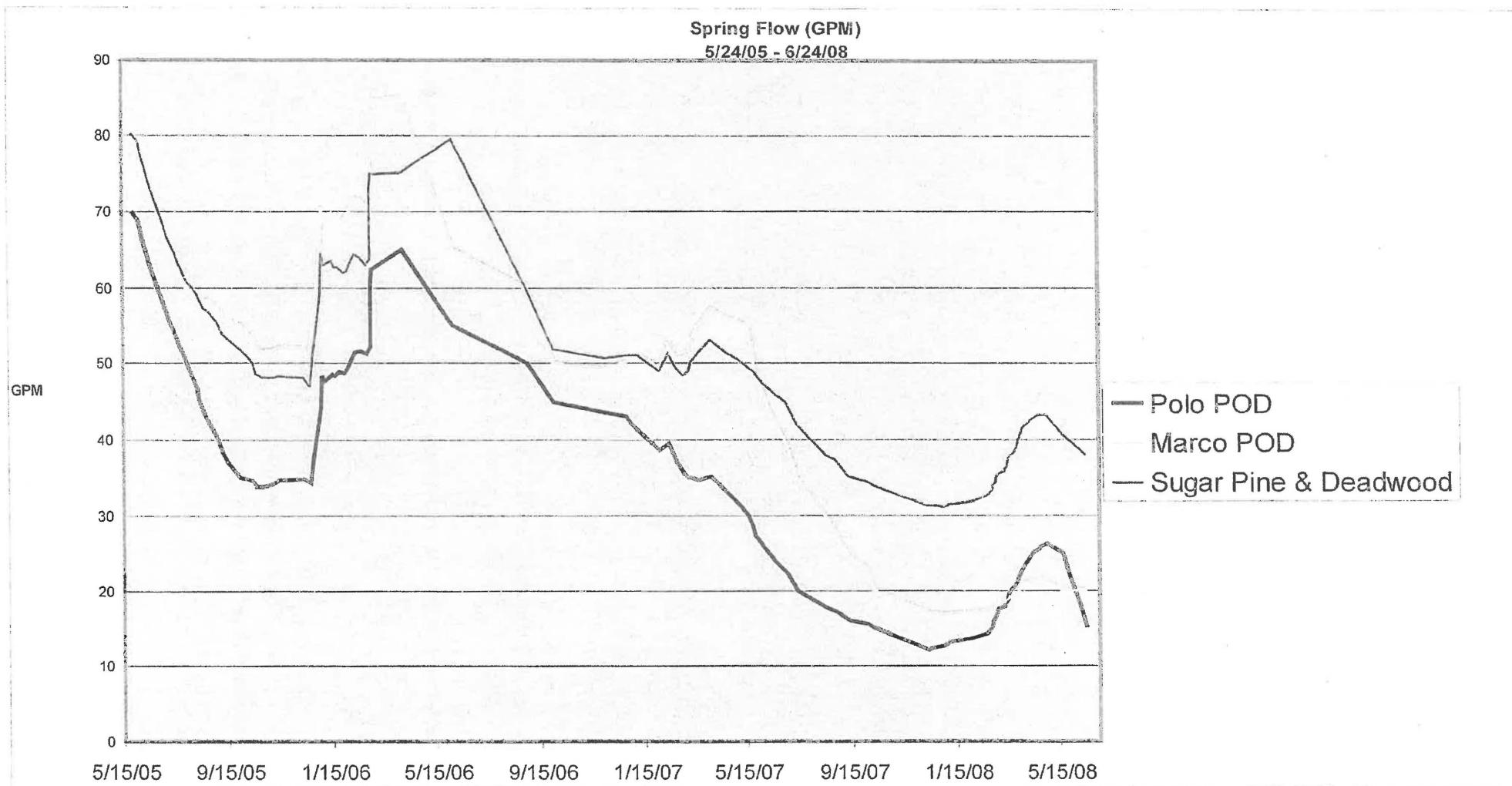


Figure 9. Graph Showing Effect of Spring Flow on Anticipated Diversion Volumes for Marco Spring

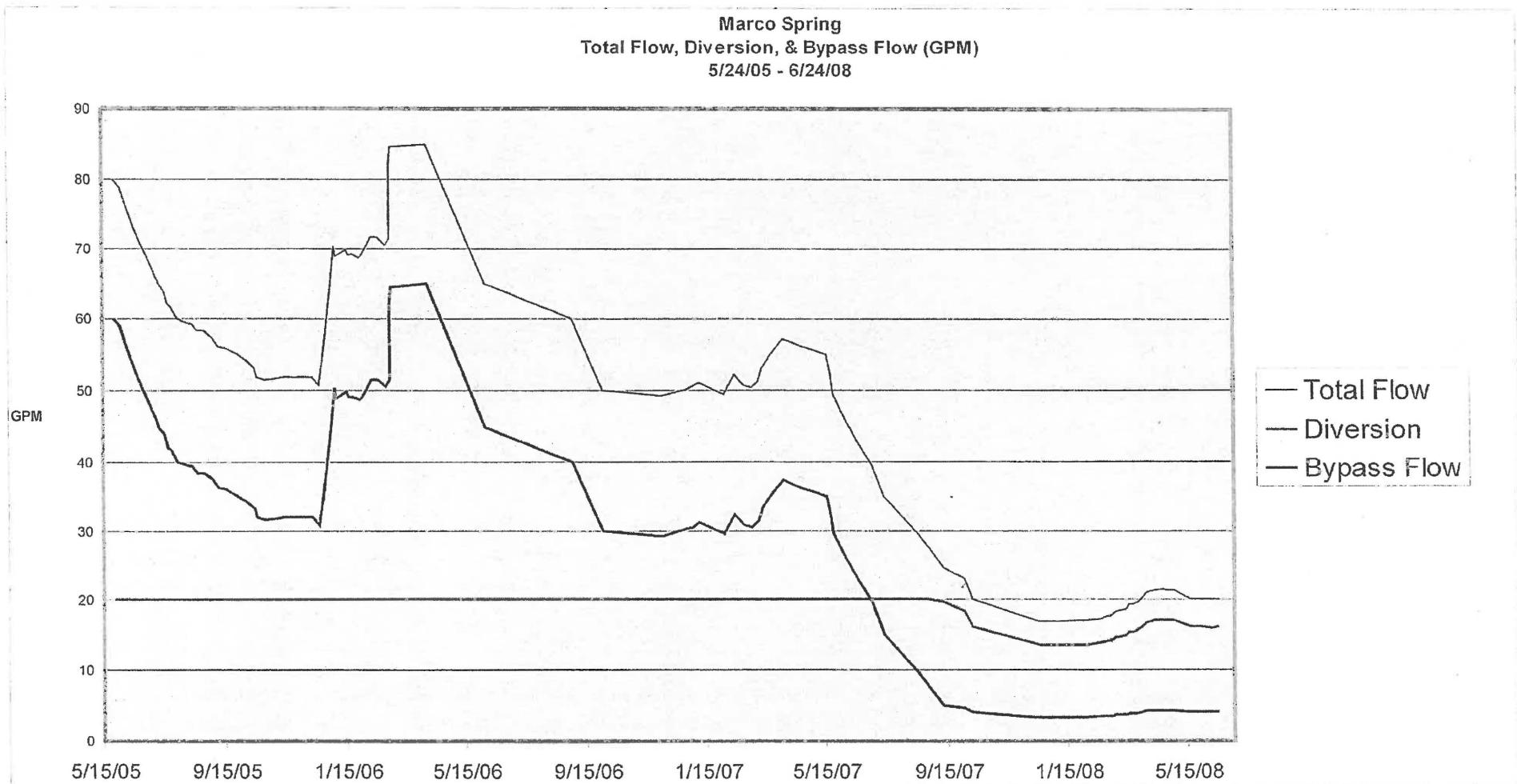
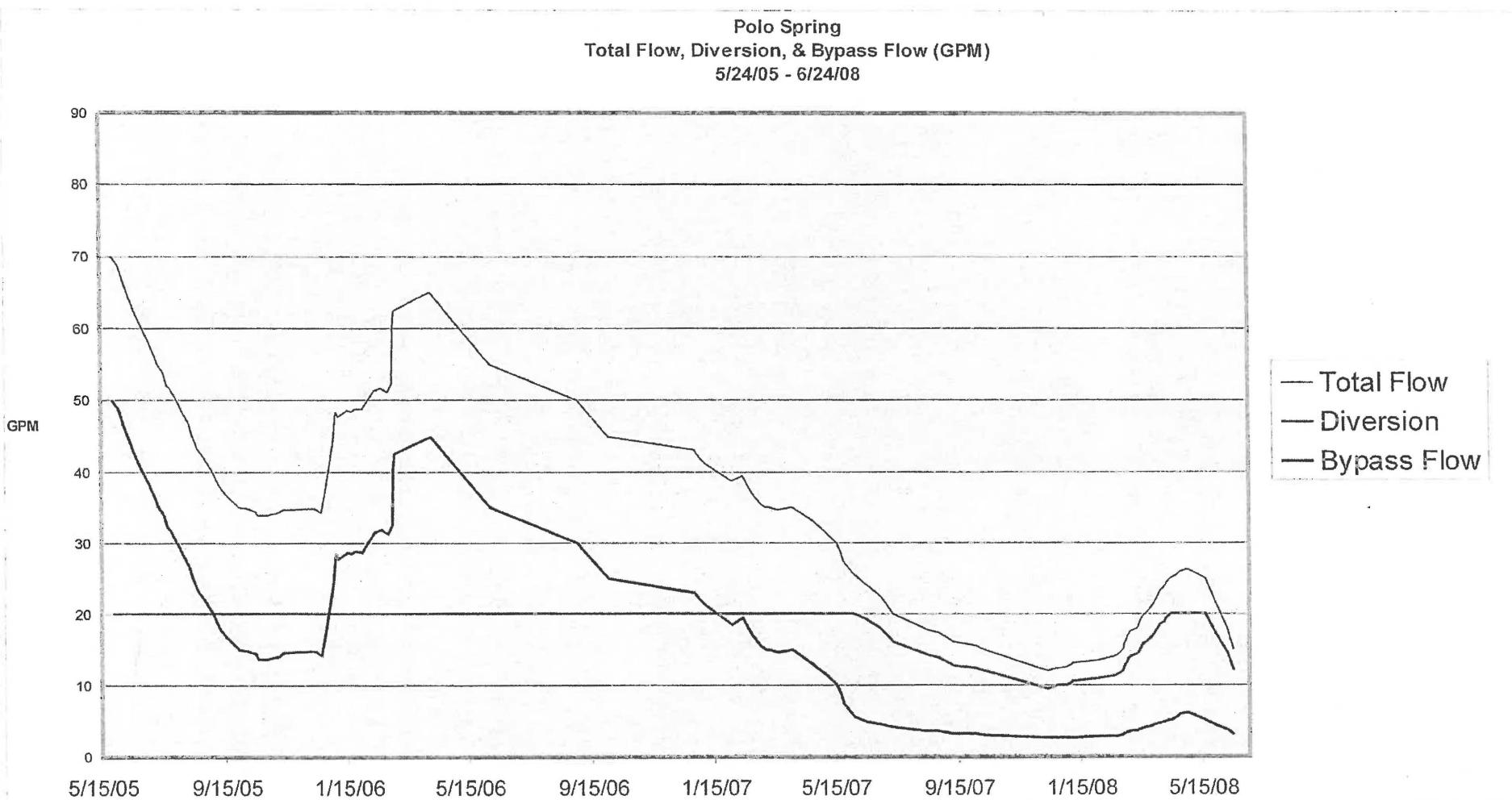


Figure 10. Graph Showing Effect of Spring Flow on Anticipated Diversion Volumes for Polo Spring



APPENDIX A

Runoff Coefficient for Undeveloped Areas

	Watershed Types			
	Extreme	High	Normal	Low
Relief	0.28 – 0.35 Steep, rugged terrain with average slopes above 30%	0.20 – 0.28 Hilly, with average slopes of 10 to 30%	0.14 – 0.20 Rolling with average slope of 5 to 10%	0.08 – 0.14 Relatively flat land, with average slope of 0 to 5%
Soil Saturation	0.12 – 0.16 No effective soil cover; either rock or thin soil mantle of negligible infiltration capacity	0.08 – 0.12 Slow to take up water; clay or loam soil of low infiltration capacity; imperfectly or poorly drained	0.06 – 0.08 Normal; well-drained, high or medium-textured soils, sandy loams, silt and silty loams.	0.04 – 0.06 High; deep sand or other soil that takes up water readily, very high level drained soils.
Vegetal Cover	0.12 – 0.16 No effective plant cover, bare, or very sparse cover	0.08 – 0.12 Poor to fair; clean cultivation crops, or poor natural cover, less than 20% of drainage area over good cover	0.06 – 0.08 Fair to good; about 50% of area in good grassland or woodland, not more than 50% of area in cultivated crops	0.04 – 0.06 Good to excellent; about 90% of drainage area in good grassland, woodland or equivalent cover
Surface Storage	0.10 – 0.12 Negligible surface depression few and shallow; drainage ways steep and small, no marshes	0.08 – 0.10 Low; very well defined system of drainage ways; no ponds or marshes	0.06 – 0.08 Normal; considerable surface depression storage, lakes and pond marshes	0.04 – 0.06 High; surface storage high; drainage system not sharply defined, large floodplain storage or large number of pond marshes

Example 1: The watershed above project site consisting of:

- 1) Hilly terrain with average slope of 15%,
- 2) Well-drained gravelly loams,
- 3) Planted with grapes, and
- 4) Low, well-defined

Find the runoff coefficient, C, for the above watershed.

<u>Solutions:</u>	
Relief =	0.25
Soil infiltration =	0.11
Vegetal Cover =	0.07
Surface storage =	0.09

C =	0.52

Reference Source: California Department of Transportation, *Highway Design Manual*, July 1, 1995, pp. 810-816.

APPENDIX B
Demand above POI A

Case A

Water Right ID	Source	Direct Diversion Rate (cfs)	Direct Diversion Season	Adjusted Direct Diversion Amount Jan 1-Dec 31 (af)*	Face Value Storage Amount (af)	Storage Season	Adjusted Storage Amount Oct. 1-Mar. 31 (af)*	Cumulative Adjusted Diversion Amount Jan. 1-Dec. 31 (af)	Purpose of Use Code**
A020636-01	Tributary to FAHEY CREEK, thence HULL CREEK, CLAVEY RIVER	500 Gallons/Day (0.0008 cfs)	May 1-December 1	0.38	0	NA	NA	0.38	D
A018652-01*	NA	NA	NA	NA	NA	NA	NA	NA	NA
	U.S. Forest Service Reserved Right		May 1-Oct 1	1.34	0	NA	NA	1.34	D, S
39491	Marco Spring	20 gallons/min (0.045 cfs)	January 1-December 31	32.25	0	0	0	32.25	Z
Totals:				33.97				33.97	

*Water right revoked on 7/17/2002.

**B-Mining, C-Milling, D-Domestic, E-Fire Protection, G-Dust Control, H-Fish Culture, I-Irrigation, J-Industrial, K-Incidental Power, L-Heat Protection, M-Municipal, N-Frost Protection, P-Power, R-Recreational, S-Stockwatering, T-Snow Making, W-Fish and Wildlife Protection and/or Enhancement, Z-Other.

APPENDIX C
Demand above POI B

Case A

Water Right ID	Source	Direct Diversion Rate (cfs)	Direct Diversion Season	Adjusted Direct Diversion Amount Jan 1-Dec 31 (af)*	Face Value Storage Amount (af)	Storage Season	Adjusted Storage Amount Oct. 1-Mar. 31 (af)*	Cumulative Adjusted Diversion Amount Jan. 1-Dec. 31 (af)	Purpose of Use Code**
A020636-01	Tributary to FAHEY CREEK, thence HULL CREEK, CLAVEY RIVER	500 Gallons/Day (0.0008 cfs)	May 1-December 1	0.38	0	NA	NA	0.38	D
A018652-01*	NA	NA	NA	NA	NA	NA	NA	NA	NA
	U.S. Forest Service Reserved Right		May 1-Oct 1	1.34	0	NA	NA	1.34	D, S
39491	Marco Spring	20 gallons/min (0.045 cfs)	January 1-December 31	32.25	0	0	0	32.25	Z
39491	Polo Spring	20 gallons/min (0.045 cfs)	January 1-December 31	32.25	0	0	0	32.25	Z
Totals:				66.22				66.22	

*Water right revoked on 7/17/2002.

**B-Mining, C-Milling, D-Domestic, E-Fire Protection, G-Dust Control, H-Fish Culture, I-Irrigation, J-Industrial, K-Incidental Power, L-Heat Protection, M-Municipal, N-Frost Protection, P-Power, R-Recreational, S-Stockwatering, T-Snow Making, W-Fish and Wildlife Protection and/or Enhancement, Z-Other.

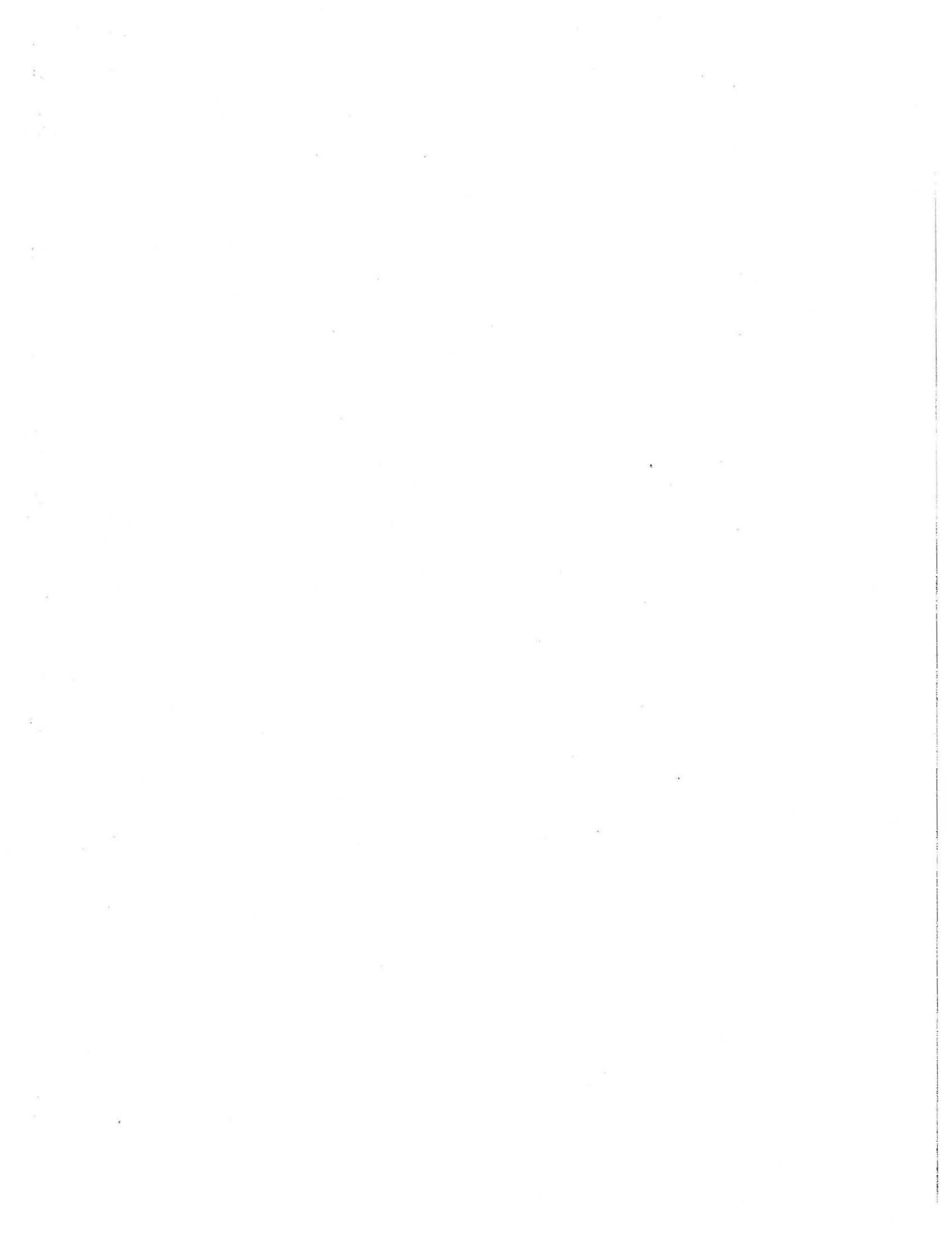
APPENDIX D
Demand above POI C

Case A

Water Right ID	Source	Direct Diversion Rate (cfs)	Direct Diversion Season	Adjusted Direct Diversion Amount Jan 1-Dec 31.(af)*	Face Value Storage Amount (af)	Storage Season	Adjusted Storage Amount Oct. 1-Mar. 31 (af)*	Cumulative Adjusted Diversion Amount Jan. 1-Dec. 31 (af)	Purpose of Use Code**
A020636-01	Tributary to FAHEY CREEK, thence HULL CREEK, CLAVEY RIVER	500 Gallons/Day (0.0008 cfs)	May 1-December 1	0.38	0	NA	NA	0.38	D
A018652-01*	NA	NA	NA	NA	NA	NA	NA	NA	NA
	U.S. Forest Service Reserved Right		May 1-Oct 1	1.34	0	NA	NA	1.34	D, S
39491	Marco Spring	20 gallons/min (0.045 cfs)	January 1-December 31	32.25	0	0	0	32.25	Z
39491	Polo Spring	20 gallons/min (0.045 cfs)	January 1-December 31	32.25	0	0	0	32.25	Z
Totals:				66.22				66.22	

*Water right revoked on 7/17/2002.

**B-Mining, C-Milling, D-Domestic, E-Fire Protection, G-Dust Control, H-Fish Culture, I-Irrigation, J-Industrial, K-Incidental Power, L-Heat Protection, M-Municipal, N-Frost Protection, P-Power, R-Recreational, S-Stockwatering, T-Snow Making, W-Fish and Wildlife Protection and/or Enhancement, Z-Other.



APPENDIX E
Demand above POI D

Case A

Water Right ID	Source	Direct Diversion Rate (cfs)	Direct Diversion Season	Adjusted Direct Diversion Amount Jan 1-Dec 31 (af)*	Face Value Storage Amount (af)	Storage Season	Adjusted Storage Amount Oct. 1-Mar. 31 (af)*	Cumulative Adjusted Diversion Amount Jan. 1-Dec. 31 (af)	Purpose of Use Code**
A020636-01	Tributary to FAHEY CREEK, thence HULL CREEK, CLAVEY RIVER	500 Gallons/Day (0.0008 cfs)	May 1-December 1	0.38	0	NA	NA	0.38	D
A018652-01*	NA	NA	NA	NA	NA	NA	NA	NA	NA
	U.S. Forest Service Reserved Right		May 1-Oct 1	1.34	0	NA	NA	1.34	D, S
39491	Marco Spring	20 gallons/min (0.045 cfs)	January 1-December 31	32.25	0	0	0	32.25	Z
39491	Polo Spring	20 gallons/min (0.045 cfs)	January 1-December 31	32.25	0	0	0	32.25	Z
Totals:				66.22				66.22	

*Water right revoked on 7/17/2002.

**B-Mining, C-Milling, D-Domestic, E-Fire Protection, G-Dust Control, H-Fish Culture, I-Irrigation, J-Industrial, K-Incidental Power, L-Heat Protection, M-Municipal, N-Frost Protection, P-Power, R-Recreational, S-Stockwatering, T-Snow Making, W-Fish and Wildlife Protection and/or Enhancement, Z-Other.

APPENDIX F
Flow Records for
Clavey River Gage #11283500
From USGS Archive Files

Gage	Year	Day	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	
11283500	1960	1		17	13	13	10	170	85	412	405	213	25	13	7.5
11283500	1960	2		17	14	14	13	235	83	470	455	218	25	13	7.5
11283500	1960	3		16	14	14	16	110	83	543	433	208	25	12	8.1
11283500	1960	4		16	14	14	14	90	83	585	373	171	24	12	8.5
11283500	1960	5		16	14	13	16	100	93	594	349	163	23	12	8.1
11283500	1960	6		16	14	13	17	110	131	627	396	142	23	12	7.9
11283500	1960	7		16	14	13	17	100	236	670	490	129	24	11	7.5
11283500	1960	8		16	14	13	18	1020	460	576	493	112	24	11	7.4
11283500	1960	9		16	14	13	19	800	318	561	505	104	22	10	7.4
11283500	1960	10		16	14	14	44	310	251	597	531	96	21	10	9.5
11283500	1960	11		16	14	13	33	210	240	573	549	91	20	9.7	13
11283500	1960	12		16	14	13	27	180	270	370	576	84	20	9.5	12
11283500	1960	13		15	14	16	19	160	368	354	513	76	19	9.3	10
11283500	1960	14		15	14	12	22	148	316	416	440	70	19	8.9	8.3
11283500	1960	15		15	14	15	21	137	271	390	399	64	18	8.7	7.5
11283500	1960	16		15	14	15	18	130	247	351	377	59	17	8.7	7.9
11283500	1960	17		14	14	15	21	125	263	362	334	55	17	8.9	8.1
11283500	1960	18		14	14	15	21	130	334	364	324	51	16	8.3	7.9
11283500	1960	19		14	14	15	21	120	392	366	299	47	15	7.9	7.4
11283500	1960	20		14	14	14	21	110	421	401	292	43	15	7.7	7.2
11283500	1960	21		14	14	15	23	105	438	421	295	40	14	7.4	6.8
11283500	1960	22		14	14	15	42	100	453	399	235	37	15	7.4	6.8
11283500	1960	23		14	14	15	35	95	440	284	201	35	14	7.7	7.2
11283500	1960	24		14	14	26	40	92	453	259	187	33	14	8.3	7
11283500	1960	25		14	14	60	129	90	520	235	198	32	14	8.5	6.8
11283500	1960	26		14	14	26	152	90	510	221	187	31	14	8.1	6.6
11283500	1960	27		14	14	20	96	85	834	283	208	30	14	8.1	6.6
11283500	1960	28		14	14	20	65	85	797	273	219	28	14	7.9	7.7
11283500	1960	29		14	14	18	53	85	520	267	230	27	13	7.9	7.4
11283500	1960	30		13	13	17	47		518	326	213	26	13	7.7	7.2
11283500	1960	31		13		17	46		443		213		14	7.5	

14.903226 13.93333 16.96774 36.64516 183.5172 350.6774 418.3333 352.2258 83.83333 18.22581 9.358065 7.96

Gage	Year	Day	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug
11283500	1961	1	7.4	11	142	24	62	58	193	246	131	15	4.4	3.9
11283500	1961	2	7.7	11	220	22	72	64	237	203	152	14	4.4	3.8
11283500	1961	3	7.7	13	89	23	85	70	360	197	136	15	4.4	3.7
11283500	1961	4	7.4	21	60	26	68	68	392	198	122	18	4.4	3.6
11283500	1961	5	7.4	17	48	23	62	66	360	163	115	19	4.4	3.6
11283500	1961	6	12	20	39	24	58	70	311	155	119	16	4.4	3.6
11283500	1961	7	17	27	35	25	60	60	267	187	111	15	4.3	3.5
11283500	1961	8	14	19	35	23	57	71	204	263	103	14	4.2	3.5
11283500	1961	9	14	17	35	24	60	77	218	260	94	13	4.1	3.6
11283500	1961	10	13	16	33	24	80	72	190	284	85	12	4	3.7
11283500	1961	11	13	16	34	23	175	76	187	246	81	11	4	3.7
11283500	1961	12	13	28	29	23	152	74	236	195	70	10	4.3	3.6
11283500	1961	13	12	45	29	23	108	74	171	172	63	11	4.6	3.6
11283500	1961	14	12	37	31	25	90	81	181	184	59	9.9	5	3.6
11283500	1961	15	12	28	31	24	93	115	193	210	51	9.1	5	3.6
11283500	1961	16	12	24	30	24	87	90	247	193	44	8.5	4.6	4.2
11283500	1961	17	12	24	31	26	84	115	249	193	39	7.9	4.1	9.9
11283500	1961	18	12	26	31	23	76	110	251	204	42	7.7	4.2	9.1
11283500	1961	19	11	33	30	24	66	110	179	189	41	7	4.1	7.4
11283500	1961	20	11	28	29	24	70	123	134	189	37	6.7	4.2	6.4
11283500	1961	21	11	26	31	26	73	165	118	201	32	6.2	4.6	5.8
11283500	1961	22	11	25	31	27	85	178	126	190	28	6.2	4	5.9
11283500	1961	23	11	24	32	25	77	249	130	179	24	6.1	3.8	5.9
11283500	1961	24	11	23	34	26	73	216	118	156	23	5.8	3.8	6.1
11283500	1961	25	11	23	34	26	68	171	125	163	21	5.5	3.6	5.8
11283500	1961	26	11	31	34	58	65	143	147	154	20	5.4	3.6	5.4
11283500	1961	27	11	26	30	53	60	145	186	123	19	5	3.7	5.1
11283500	1961	28	11	26	27	41	57	135	223	123	18	4.9	3.9	5
11283500	1961	29	11	26	25	42		131	267	115	16	4.6	4.3	5.8
11283500	1961	30	11	28	28	47		145	262	101	16	4.4	4	7
11283500	1961	31	11		26	50		185		105		4.4	3.9	
11.245161														
11283500	1962	1	6.2	7.6	60	26	47	124	526	755	600	121	21	11
11283500	1962	2	5.7	7.6	95	24	52	126	548	899	664	112	20	11
11283500	1962	3	5.2	7.8	47	25	54	125	590	1020	616	107	20	10
11283500	1962	4	5.1	7.8	31	23	54	124	706	1120	459	98	20	10
11283500	1962	5	4.9	7.6	26	24	53	135	854	1180	444	92	21	10
11283500	1962	6	4.8	7.4	24	25	53	261	938	1120	462	84	21	10
11283500	1962	7	4.7	7.2	21	25	102	220	1030	1050	492	75	20	10
11283500	1962	8	4.6	7.2	21	32	212	194	1050	1060	500	70	20	10
11283500	1962	9	4.7	7	18	40	1830	182	1130	1000	502	65	20	9.9
11283500	1962	10	4.9	7	20	36	1540	162	1090	874	492	60	21	9.9
11283500	1962	11	5.4	7	16	33	717	159	1050	644	451	57	19	9.9
11283500	1962	12	5.7	7	19	30	435	143	1150	580	418	59	18	9.9
11283500	1962	13	5.7	7	17	31	468	144	1240	462	396	62	17	9.9
11283500	1962	14	5.5	7	18	20	587	144	1330	420	368	55	16	10
11283500	1962	15	5.2	7	17	22	1070	142	1380	378	320	50	15	10
11283500	1962	16	5	7	17	24	636	145	1250	440	301	46	15	10
11283500	1962	17	4.9	7	18	22	404	138	1160	490	313	42	15	9.7
11283500	1962	18	4.8	7	21	24	317	135	1210	502	333	39	15	9.3
11283500	1962	19	4.9	7.4	22	28	274	139	1150	519	322	37	14	9.1
11283500	1962	20	4.9	15	24	36	236	170	812	480	317	35	14	9.3
11283500	1962	21	5.5	14	26	26	202	160	812	394	290	33	14	9.3
11283500	1962	22	6.9	12	25	25	188	192	983	485	269	31	14	9.5
11283500	1962	23	7	12	26	27	175	186	1090	538	248	29	13	9.3
11283500	1962	24	6.9	12	28	25	167	180	1100	462	220	28	13	8.9
11283500	1962	25	6.7	14	27	25	137	202	1000	411	201	26	12	8.9
11283500	1962	26	6.9	45	30	26	149	238	890	362	186	25	12	10
11283500	1962	27	6.9	27	27	28	123	278	915	352	168	24	11	9.9
11283500	1962	28	11	19	26	31	133	333	1160	402	157	24	11	11
11283500	1962	29	11	18	26	34		407	806	413	145	23	11	11
11283500	1962	30	8.7	44	25	37		464	680	504	134	22	11	11
11283500	1962	31	7.8		25	42		492		572		22	11	
11283500	1963	1	10	16	17	20	9980	160	336	960	567	158	41	22
11283500	1963	2	9.9	16	17	20	1880	154	346	992	582	155	40	21
11283500	1963	3	9.7	16	19	20	852	143	280	1040	538	147	40	20

11283500	1963	4	10	15	21	20	647	126	302	1050	404	137	39	19
11283500	1963	5	10	15	23	18	495	125	388	1080	435	130	38	20
11283500	1963	6	11	15	21	19	402	124	802	1080	485	125	37	20
11283500	1963	7	11	15	20	18	350	122	1550	1120	442	122	36	21
11283500	1963	8	11	15	20	18	322	119	1000	1910	468	117	35	19
11283500	1963	9	11	15	19	19	288	122	730	1940	442	110	34	18
11283500	1963	10	11	15	18	18	372	122	590	1250	455	101	34	18
11283500	1963	11	11	15	18	16	304	115	507	1010	507	94	33	17
11283500	1963	12	13	15	18	13	267	110	488	890	448	87	33	17
11283500	1963	13	22	15	17	13	427	107	500	866	409	83	31	23
11283500	1963	14	183	16	17	17	471	108	1180	784	446	79	29	22
11283500	1963	15	72	17	23	17	356	114	1110	852	437	75	29	20
11283500	1963	16	41	17	424	17	317	118	787	1080	429	71	27	19
11283500	1963	17	31	16	162	16	282	101	636	1140	400	68	26	20
11283500	1963	18	25	16	84	16	255	130	551	1200	366	65	25	21
11283500	1963	19	24	16	73	15	245	131	536	1250	322	64	25	22
11283500	1963	20	26	16	56	16	235	152	500	1180	327	61	24	22
11283500	1963	21	26	16	45	16	225	195	466	1050	293	58	24	22
11283500	1963	22	24	16	37	17	208	200	442	1070	253	57	24	22
11283500	1963	23	23	15	33	17	190	239	457	1000	234	55	24	21
11283500	1963	24	22	15	28	17	183	194	480	814	212	53	24	21
11283500	1963	25	21	15	22	16	179	218	504	838	208	51	24	20
11283500	1963	26	20	15	21	16	186	217	462	838	214	50	23	19
11283500	1963	27	19	24	20	16	188	296	426	836	212	48	22	18
11283500	1963	28	18	23	23	16	168	669	464	1060	203	47	22	18
11283500	1963	29	17	19	22	18		462	644	650	167	45	21	17
11283500	1963	30	17	17	22	676		386	830	633	157	44	21	17
11283500	1963	31	16		21	6410		382		600		43	24	
11283500	1964	1	17	22	111	60	102	107	358	424	280	66	18	19
11283500	1964	2	17	23	102	64	108	105	308	322	256	62	18	17
11283500	1964	3	16	25	95	58	108	93	275	286	238	60	18	16
11283500	1964	4	17	27	89	58	109	106	278	270	232	57	18	15
11283500	1964	5	17	42	87	48	119	115	278	262	209	55	17	14
11283500	1964	6	18	352	83	60	123	112	249	255	203	53	16	13
11283500	1964	7	18	115	78	58	117	101	242	249	252	50	16	13
11283500	1964	8	17	78	77	54	114	89	267	283	245	46	16	12
11283500	1964	9	18	90	85	50	119	101	322	331	309	43	15	11
11283500	1964	10	18	74	68	54	124	93	358	468	285	41	15	11
11283500	1964	11	45	60	72	45	125	92	402	574	311	39	14	11
11283500	1964	12	41	52	70	52	114	108	433	616	366	37	14	10
11283500	1964	13	27	49	73	43	108	108	464	644	270	35	14	10
11283500	1964	14	24	70	68	51	98	103	533	608	227	33	14	10
11283500	1964	15	23	1200	70	40	106	124	572	559	213	32	13	9.9
11283500	1964	16	22	234	67	48	94	139	569	548	191	32	13	9.7
11283500	1964	17	21	135	66	54	92	153	533	507	198	31	13	9.5
11283500	1964	18	22	101	66	65	93	183	457	509	170	29	13	9.3
11283500	1964	19	21	97	64	69	99	197	394	500	152	28	12	9.3
11283500	1964	20	21	189	72	91	110	214	344	502	142	27	12	9.1
11283500	1964	21	21	135	71	175	114	225	354	446	133	26	12	8.9
11283500	1964	22	21	102	64	83	120	198	368	374	125	25	12	8.7
11283500	1964	23	23	161	62	80	117	179	364	374	117	24	12	8.5
11283500	1964	24	27	227	62	100	120	170	294	352	107	23	12	8.4
11283500	1964	25	24	151	60	107	122	150	272	352	99	23	11	8.2
11283500	1964	26	24	132	60	107	107	168	274	364	90	22	11	8.2
11283500	1964	27	22	129	58	106	108	190	362	348	83	21	11	8
11283500	1964	28	22	125	58	101	109	234	528	327	78	22	11	7.9
11283500	1964	29	21	122	60	101	106	267	466	277	74	21	11	8
11283500	1964	30	23	117	60	104		294	444	278	69	20	11	8.2
11283500	1964	31	23		60	100		326		272		19	12	
11283500	1965	1	8.2	28	77	512	502	421	430	1310	668	254	45	27
11283500	1965	2	8	36	114	488	495	399	430	1050	560	229	43	27
11283500	1965	3	7.6	24	111	465	485	395	407	760	582	234	41	26
11283500	1965	4	7.6	22	80	442	480	393	411	685	670	233	39	25
11283500	1965	5	7.5	21	76	521	610	375	413	692	718	203	37	25
11283500	1965	6	7.6	19	61	1790	672	373	430	668	675	199	36	25
11283500	1965	7	7.6	17	66	1670	552	349	415	578	618	187	34	28
11283500	1965	8	7.6	17	62	838	508	331	421	542	608	165	33	36
11283500	1965	9	8	58	68	662	475	322	428	542	468	151	32	39

11283500	1965	10	8.2	92	91	600	442	325	413	620	562	139	33	33
11283500	1965	11	8.2	67	179	548	419	322	397	655	612	126	37	29
11283500	1965	12	8	248	184	512	399	345	387	736	590	116	83	27
11283500	1965	13	7.6	128	108	475	389	325	389	832	512	110	129	25
11283500	1965	14	7.6	66	98	458	381	318	399	826	425	105	74	24
11283500	1965	15	7.6	58	86	465	367	318	438	829	377	102	94	24
11283500	1965	16	7.6	50	72	460	353	318	500	1000	351	121	214	23
11283500	1965	17	8	46	66	455	351	327	510	1140	385	109	215	22
11283500	1965	18	8.5	38	65	468	359	329	548	1080	308	129	390	22
11283500	1965	19	8.4	40	163	515	379	347	695	1040	333	107	107	22
11283500	1965	20	8.2	41	368	542	395	369	984	931	397	93	75	22
11283500	1965	21	8.2	40	430	515	413	403	1230	948	452	84	59	22
11283500	1965	22	8.2	43	2460	490	425	417	1230	682	375	76	50	22
11283500	1965	23	8	44	8580	536	403	450	1070	578	339	69	45	22
11283500	1965	24	8.2	46	7810	979	389	440	1100	585	290	64	42	21
11283500	1965	25	8.5	54	2540	658	389	391	1260	570	306	61	39	20
11283500	1965	26	8.7	90	1640	575	397	389	1260	650	274	58	36	20
11283500	1965	27	8.9	90	2020	535	490	438	1360	660	241	56	33	21
11283500	1965	28	11	70	1170	502	470	413	1450	675	254	53	31	22
11283500	1965	29	51	67	836	480		413	1470	754	254	50	30	22
11283500	1965	30	31	72	690	478		423	1460	754	264	48	29	21
11283500	1965	31	19		594	498		432		721		47	27	
11283500	1966	1	20	18	181	138	115	147	775	442	106	26	15	9.3
11283500	1966	2	20	18	175	129	103	142	760	430	96	25	14	8.9
11283500	1966	3	19	18	180	129	115	130	690	468	90	24	13	8.4
11283500	1966	4	19	18	193	123	112	128	742	448	86	24	12	8
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11283500	1966	6	19	18	179	151	224	138	692	438	81	22	12	7.8
11283500	1966	7	19	18	171	160	163	153	652	425	89	22	11	7.7
11283500	1966	8	18	18	164	164	147	181	632	419	100	21	11	7.7
11283500	1966	9	18	18	159	162	143	205	618	381	107	24	11	7.8
11283500	1966	10	18	19	154	153	134	327	718	535	94	22	11	7.7
11283500	1966	11	18	19	147	145	113	385	595	417	81	21	10	7.7
11283500	1966	12	18	20	155	138	130	369	542	355	75	20	10	7.9
11283500	1966	13	18	31	139	136	113	508	492	318	69	20	10	8.3
11283500	1966	14	19	228	138	135	116	530	470	319	63	20	10	8.8
11283500	1966	15	26	195	118	138	115	482	502	292	58	19	10	9
11283500	1966	16	24	199	110	138	117	438	540	283	54	18	9	9
11283500	1966	17	22	548	100	133	119	389	565	276	50	18	9.2	8.6
11283500	1966	18	22	1130	103	127	123	381	575	268	47	17	9	9.2
11283500	1966	19	21	605	103	129	125	393	448	272	44	17	8.8	13
11283500	1966	20	21	314	105	116	123	375	395	255	42	16	8.6	13
11283500	1966	21	20	215	107	115	127	365	371	248	39	16	8.4	12
11283500	1966	22	20	172	108	120	136	381	371	234	39	15	8.5	10
11283500	1966	23	19	574	88	114	152	435	381	215	37	15	8.5	9.6
11283500	1966	24	19	721	102	114	163	488	435	198	36	14	8.4	9.3
11283500	1966	25	18	423	103	108	143	505	488	184	35	14	8.4	9
11283500	1966	26	18	304	100	110	149	525	515	177	33	14	8.2	9
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11283500	1966	28	18	229	114	102	145	622	468	150	29	13	8.6	8.7
11283500	1966	29	18	213	201	108		658	432	139	28	13	8.6	8.4
11283500	1966	30	18	197	204	120		688	435	125	27	13	8.7	8.1
11283500	1966	31	18		166	116		745		116		15	9.2	
11283500	1967	1	8.1	9.3	201	113	502	254	547	402	935	731	92	33
11283500	1967	2	8.3	9.2	593	109	404	261	510	451	804	683	86	32
11283500	1967	3	8.5	9.3	865	108	357	278	483	525	755	626	81	33
11283500	1967	4	8.7	9.3	353	107	327	255	493	580	949	557	77	33
11283500	1967	5	9	9.3	866	108	325	230	478	580	1160	502	73	33
11283500	1967	6	8.9	12	3590	90	329	226	500	646	947	460	68	31
11283500	1967	7	8.8	27	1340	99	333	234	573	893	1090	423	65	30
11283500	1967	8	8.8	19	590	97	342	257	521	1250	1130	395	62	30
11283500	1967	9	8.8	15	434	91	342	271	502	1460	1120	366	60	29
11283500	1967	10	8.6	14	379	93	358	271	513	1420	1110	333	57	29
11283500	1967	11	8.4	13	332	94	363	262	494	1070	1090	317	55	29
11283500	1967	12	8.5	13	295	97	359	385	465	901	1080	317	52	28
11283500	1967	13	8.9	13	277	99	377	353	481	879	1010	312	50	27
11283500	1967	14	9.1	13	251	103	367	314	511	999	987	298	47	27
11283500	1967	15	9.3	13	231	105	324	322	496	1370	1030	285	45	26

11283500	1967	16	9.5	148	225	106	305	3520	454	1830	1130	245	44	26
11283500	1967	17	9.6	127	217	101	291	3020	452	2170	1210	237	43	25
11283500	1967	18	9.6	60	211	99	292	1750	490	2250	1270	224	41	46
11283500	1967	19	9.6	42	208	96	295	1250	471	2250	1170	208	40	41
11283500	1967	20	9.5	288	208	102	277	990	454	2540	1050	188	38	32
11283500	1967	21	9.5	202	190	313	265	873	444	2900	1060	172	38	30
11283500	1967	22	9.7	176	171	377	261	873	430	2960	1050	162	37	28
11283500	1967	23	9.8	102	165	238	255	848	426	2790	965	160	36	28
11283500	1967	24	9.6	74	153	216	249	759	431	2560	934	150	35	42
11283500	1967	25	9.6	60	147	188	260	693	421	2300	949	142	40	32
11283500	1967	26	9.4	57	139	186	233	636	424	2070	901	130	71	30
11283500	1967	27	9.3	54	115	213	241	601	453	1940	854	122	59	28
11283500	1967	28	9.5	353	125	261	240	802	426	1870	801	116	45	27
11283500	1967	29	9.6	803	130	587		755	403	1560	811	112	40	27
11283500	1967	30	9.4	312	124	722		628	398	1400	786	106	37	26
11283500	1967	31	9.4		115	726		593		1180		99	34	
11283500	1968	1	26	20	33	47	75	352	533	420	173	26	13	9.3
11283500	1968	2	26	20	31	43	85	309	455	420	173	25	12	9.4
11283500	1968	3	45	20	34	37	92	301	379	422	169	24	11	8
11283500	1968	4	35	20	37	39	97	302	381	401	153	24	11	7.7
11283500	1968	5	31	20	129	37	101	302	398	379	142	23	10	7.7
11283500	1968	6	30	20	60	37	100	274	366	325	116	22	10	7.5
11283500	1968	7	28	20	62	36	98	255	360	299	110	21	9.8	7
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11283500	1968	9	27	20	47	36	119	272	421	298	96	21	9.2	6.6
11283500	1968	10	26	19	44	49	125	245	476	270	95	20	9	6.7
11283500	1968	11	26	19	43	46	113	231	522	265	95	19	8.8	6.8
11283500	1968	12	24	19	42	43	105	230	505	281	91	18	9	6.8
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11283500	1968	19	22	54	38	84	296	219	301	306	55	16	11	6.2
11283500	1968	20	22	47	36	78	888	214	302	311	51	15	22	6.2
11283500	1968	21	21	35	36	80	812	227	288	338	46	14	21	6.6
11283500	1968	22	22	30	36	85	571	243	269	267	43	14	20	7
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11283500	1968	27	21	25	53	82	403	295	434	235	30	12	11	6.2
11283500	1968	28	21	26	56	66	383	334	441	245	28	12	10	6
11283500	1968	29	21	28	62	73	359	412	462	238	27	12	9.7	6
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11283500	1968	31	20		51	64		477		181		12	8.5	
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11283500	1969	3	6.7	514	52	104	600	353	1180	1300	1400	355	59	23
11283500	1969	4	6.7	210	49	112	572	337	1080	1190	1290	326	56	23
11283500	1969	5	8.3	102	48	125	573	329	1720	1310	1220	312	53	23
11283500	1969	6	14	76	51	141	576	333	1440	1630	1120	300	51	23
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11283500	1969	23	13	74	89	1350	377	490	1880	1730	588	131	29	21
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11283500	1969	25	12	71	291	4230	401	598	1220	1590	515	109	28	21
11283500	1969	26	12	57	185	4970	389	662	1140	1570	440	99	27	23
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11283500	1970	2	19	28	31	116	477	590	370	468	322	100	24	15
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11283500	1970	5	19	29	29	89	432	439	418	616	273	80	22	15
11283500	1970	6	19	102	31	91	407	441	458	630	252	75	21	15
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11283500	1970	9	19	68	34	233	383	429	443	421	648	62	18	14
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11283500	1970	27	34	34	305	1120	363	503	350	445	459	27	15	14
11283500	1970	28	33	32	211	870	425	466	321	384	267	27	15	13
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11283500	1970	30	30	31	163	638		443	344	354	131	26	15	13
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11283500	1971	4	13	22	235	109	234	185	719	508	355	126	23	15
11283500	1971	5	13	139	213	108	223	174	783	462	423	116	23	15
11283500	1971	6	13	218	185	103	216	169	770	472	446	108	22	15
11283500	1971	7	13	130	189	103	213	172	640	464	496	99	22	17
11283500	1971	8	14	79	241	105	214	173	564	484	535	91	21	16
11283500	1971	9	14	70	317	104	215	179	586	453	523	85	21	15
11283500	1971	10	16	83	237	106	229	189	637	607	464	80	20	14
11283500	1971	11	14	76	200	116	301	193	673	740	425	75	20	14
11283500	1971	12	14	91	179	127	377	259	685	754	443	71	20	14
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11283500	1971	15	14	49	137	138	427	239	704	837	403	57	18	12
11283500	1971	16	14	46	149	145	431	251	789	833	394	53	18	12
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11283500	1971	20	15	36	125	411	275	363	482	602	309	47	17	12
11283500	1971	21	20	34	123	366	260	390	445	617	298	43	16	12
11283500	1971	22	20	34	126	315	246	418	409	451	278	40	17	13
11283500	1971	23	25	32	116	278	230	448	385	491	254	37	17	12
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11283500	1971	25	20	520	108	229	224	565	369	641	226	33	16	13
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11283500	1971	27	18	221	131	241	197	1410	338	504	477	30	16	15
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11283500	1971	29	17	408	138	268		887	401	420	196	28	16	15
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11283500	1971	31	17	135	284	830	361	26	15		
11283500	1972	1	22	18	74	119	106	340	545	281	40
11283500	1972	2	19	18	76	118	102	324	313	583	35
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11283500	1972	5	17	18	63	106	168	573	494	548	185
11283500	1972	6	16	17	78	105	205	564	489	561	194
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11283500	1972	8	15	17	58	99	152	584	376	456	213
11283500	1972	9	15	17	64	98	146	651	352	442	263
11283500	1972	10	15	17	66	95	142	638	321	393	257
11283500	1972	11	14	74	60	95	143	603	355	426	199
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11283500	1972	13	14	145	54	95	153	532	354	473	150
11283500	1972	14	14	79	58	95	162	549	319	497	141
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11283500	1972	25	18	42	561	129	222	416	410	301	58
11283500	1972	26	18	41	311	118	225	431	408	323	54
11283500	1972	27	18	84	227	106	237	355	486	344	51
11283500	1972	28	18	137	178	111	266	315	543	354	47
11283500	1972	29	17	150	154	121	378	289	536	337	44
11283500	1972	30	18	99	131	110	281	498	307	53	14
11283500	1972	31	18	124	108		304	300		15	8.6
11283500	1973	1	8	15	39	73	142	503	327	998	951
11283500	1973	2	8.2	14	37	75	141	446	305	1060	751
11283500	1973	3	8.6	14	40	79	145	419	301	1170	611
11283500	1973	4	9.1	38	59	50	190	386	320	1060	567
11283500	1973	5	8.7	37	34	49	178	347	371	814	551
11283500	1973	6	8.4	24	30	58	245	346	469	732	552
11283500	1973	7	8	24	30	53	455	325	616	936	529
11283500	1973	8	8.3	32	30	69	329	316	669	1110	497
11283500	1973	9	8.8	25	30	95	266	297	743	1270	490
11283500	1973	10	13	24	32	100	566	308	747	1330	428
11283500	1973	11	18	34	33	134	550	411	813	1500	380
11283500	1973	12	14	28	34	620	422	354	944	1560	365
11283500	1973	13	12	25	33	483	359	338	923	1580	329
11283500	1973	14	13	90	31	324	336	309	696	1630	299
11283500	1973	15	15	53	32	260	300	296	645	1540	234
11283500	1973	16	16	83	33	946	271	298	600	1620	222
11283500	1973	17	17	50	278	728	250	303	676	1700	207
11283500	1973	18	16	41	478	601	239	290	728	1540	209
11283500	1973	19	16	38	464	503	233	292	673	1640	204
11283500	1973	20	18	34	387	363	235	321	651	1240	201
11283500	1973	21	19	31	256	313	240	295	648	1070	193
11283500	1973	22	19	32	314	255	232	284	750	1000	184
11283500	1973	23	16	28	270	228	228	294	928	976	172
11283500	1973	24	15	28	188	209	283	313	1150	965	150
11283500	1973	25	13	30	143	197	297	339	1270	831	144
11283500	1973	26	13	32	126	176	336	351	1450	736	140
11283500	1973	27	13	38	120	164	432	366	1570	736	144
11283500	1973	28	13	43	113	160	603	357	1540	886	134
11283500	1973	29	13	42	82	160		330	1350	936	118
11283500	1973	30	12	40	90	162		314	1090	1030	109
11283500	1973	31	12		81	150		324		864	24
11283500	1974	1	13	22	358	441	293	500	1670	956	603
11283500	1974	2	12	23	219	329	266	1270	1410	1090	547
11283500	1974	3	12	22	198	313	263	820	1120	1090	514
11283500	1974	4	12	22	178	295	255	750	925	1020	537
11283500	1974	5	12	22	158	269	247	710	790	1130	500
11283500	1974	6	12	35	147	238	228	670	700	1250	542
11283500	1974	7	16	52	145	253	229	630	675	1340	509

11283500	1974	8	35	111	145	242	221	600	682	1330	428	58	35	14
11283500	1974	9	26	70	147	219	216	550	665	1260	385	93	32	14
11283500	1974	10	21	322	150	197	217	510	600	1180	384	473	30	14
11283500	1974	11	19	1510	160	197	210	485	582	1130	369	160	29	14
11283500	1974	12	20	1820	148	237	211	510	585	1110	364	107	27	13
11283500	1974	13	18	423	167	257	196	515	598	998	334	86	26	13
11283500	1974	14	17	292	158	241	201	522	618	865	311	74	25	13
11283500	1974	15	16	206	144	278	186	555	658	904	283	66	25	13
11283500	1974	16	16	182	141	520	193	620	712	801	261	60	24	13
11283500	1974	17	15	536	163	1330	174	565	790	679	244	56	24	12
11283500	1974	18	15	670	174	1080	188	532	990	550	200	52	24	12
11283500	1974	19	15	313	155	1170	180	523	720	484	185	49	22	12
11283500	1974	20	15	241	147	835	168	520	631	431	166	46	22	11
11283500	1974	21	16	199	161	651	170	505	681	430	170	44	22	11
11283500	1974	22	18	166	183	559	177	485	815	522	172	42	21	11
11283500	1974	23	101	142	173	502	170	460	872	604	164	40	20	11
11283500	1974	24	59	145	153	453	170	455	707	662	146	39	20	11
11283500	1974	25	36	127	153	426	172	523	615	758	129	39	19	11
11283500	1974	26	33	127	153	396	179	495	572	828	121	39	19	11
11283500	1974	27	28	118	368	360	172	584	551	870	109	39	18	11
11283500	1974	28	26	119	507	345	190	780	591	822	104	38	18	11
11283500	1974	29	25	130	943	327		810	648	722	100	36	18	11
11283500	1974	30	24	130	867	314		1030	763	633	96	37	17	11
11283500	1974	31	23		553	303		950		614		35	17	
11283500	1975	1	11	45	25	32	75	370	476	737	1840	279	52	33
11283500	1975	2	13	32	25	32	94	392	446	782	1630	258	50	32
11283500	1975	3	27	28	132	36	93	367	442	946	1440	241	48	32
11283500	1975	4	19	26	406	38	117	368	413	863	1380	231	46	31
11283500	1975	5	17	25	121	37	108	427	410	689	1420	228	43	30
11283500	1975	6	15	25	79	112	104	488	372	653	1440	227	40	28
11283500	1975	7	14	24	66	169	118	601	344	704	1290	215	40	27
11283500	1975	8	14	27	57	301	143	715	329	915	1130	188	40	27
11283500	1975	9	16	27	54	159	561	532	318	1140	1060	177	39	28
11283500	1975	10	16	26	51	119	548	439	323	1330	1030	161	37	28
11283500	1975	11	16	25	52	102	330	376	318	1530	975	153	37	30
11283500	1975	12	15	24	49	91	249	334	325	1690	928	141	36	31
11283500	1975	13	14	24	59	85	326	331	368	1930	840	126	34	32
11283500	1975	14	14	23	53	84	344	310	407	2110	875	114	33	30
11283500	1975	15	13	22	51	86	242	303	404	2030	828	107	32	28
11283500	1975	16	13	22	49	87	195	314	380	1860	710	100	31	27
11283500	1975	17	12	22	51	84	165	284	354	2020	633	98	30	26
11283500	1975	18	12	22	48	87	149	272	346	2200	504	96	29	26
11283500	1975	19	12	23	47	95	157	290	352	2190	420	93	29	26
11283500	1975	20	12	22	45	98	234	327	364	1820	411	89	50	25
11283500	1975	21	12	46	42	98	196	333	422	1200	411	85	82	25
11283500	1975	22	12	68	42	99	175	342	473	1070	403	81	81	24
11283500	1975	23	12	38	29	102	168	325	516	1270	429	76	64	24
11283500	1975	24	13	33	29	101	177	343	593	1600	450	71	51	23
11283500	1975	25	13	32	38	105	194	1160	788	1730	344	66	42	23
11283500	1975	26	13	31	36	108	217	754	603	1740	306	63	40	22
11283500	1975	27	14	29	38	96	248	602	552	1670	325	59	38	22
11283500	1975	28	69	28	42	65	307	511	582	1630	316	57	37	22
11283500	1975	29	51	26	37	79		456	642	1560	315	55	36	21
11283500	1975	30	33	26	37	63		453	710	1590	296	55	35	22
11283500	1975	31	39		32	64		493		1690		53	34	
11283500	1976	1	21	126	55	29	37	175	138	294	52	16	7.4	7.8
11283500	1976	2	21	143	59	30	37	115	132	328	49	15	7.5	7.4
11283500	1976	3	21	127	64	43	37	106	141	273	46	15	7.3	7.2
11283500	1976	4	21	113	66	48	40	101	136	282	44	15	7.4	7
11283500	1976	5	21	104	62	51	38	94	123	263	42	14	7.4	7.2
11283500	1976	6	22	91	59	47	43	91	113	262	39	13	7.1	7.4
11283500	1976	7	35	81	54	44	47	96	112	249	38	13	7	7.2
11283500	1976	8	34	125	54	44	53	102	155	280	37	12	6.9	6.9
11283500	1976	9	30	100	52	47	79	106	142	344	37	11	6.8	6.6
11283500	1976	10	69	97	52	46	73	113	160	489	44	11	6.5	6.6
11283500	1976	11	278	81	54	46	69	128	161	318	49	11	6.1	22
11283500	1976	12	135	84	58	47	69	129	150	288	61	10	5.8	46
11283500	1976	13	96	84	55	44	73	131	134	270	53	9.9	5.6	34
11283500	1976	14	83	82	36	44	91	133	135	255	44	9.6	6.1	24
11283500	1976	15	78	78	42	43	85	135	183	212	38	9.3	49	18

11283500	1976	16	73	83	48	44	74	148	147	175	34	9.5	108	15
11283500	1976	17	66	92	52	45	78	167	139	167	31	9.7	45	14
11283500	1976	18	59	76	49	45	74	198	151	146	30	9.7	31	13
11283500	1976	19	52	63	46	43	103	159	209	130	28	9.7	36	12
11283500	1976	20	47	69	46	39	80	147	303	118	27	8.9	31	11
11283500	1976	21	43	60	47	40	88	149	342	110	26	8.3	24	10
11283500	1976	22	42	56	53	39	82	163	305	103	26	8	19	9.7
11283500	1976	23	43	56	46	40	77	167	284	96	25	7.9	17	9.8
11283500	1976	24	43	56	49	41	71	163	301	89	23	9.9	15	9.5
11283500	1976	25	40	51	46	35	71	169	323	85	21	9.4	14	8.8
11283500	1976	26	222	50	46	37	69	149	244	81	20	8.2	13	8.4
11283500	1976	27	494	54	46	39	70	136	195	76	19	7.4	12	8.3
11283500	1976	28	163	58	49	38	75	124	163	71	18	6.8	11	8.5
11283500	1976	29	102	44	49	37	147	117	172	64	17	6.5	9.7	8.6
11283500	1976	30	126	50	49	37	125	224	58	16	6.3	8.9	9	
11283500	1976	31	115		37	37	150		55		6.6	8.3		
11283500	1977	1	9.7	8	11	10	15	36	42	78	105	11	2	1.4
11283500	1977	2	16	8	11	20	14	30	36	91	94	9.4	1.9	1.4
11283500	1977	3	23	7.9	11	49	14	33	33	119	78	8.8	1.8	1.4
11283500	1977	4	26	7.7	11	27	14	28	36	88	66	9	1.8	1.5
11283500	1977	5	20	7.6	11	22	14	28	70	68	59	8.9	1.8	1.4
11283500	1977	6	16	7.5	10	15	14	27	112	64	57	8.4	1.8	1.4
11283500	1977	7	14	7.5	9.7	16	15	28	128	58	57	7.8	1.9	1.3
11283500	1977	8	12	7.6	9.6	14	16	30	146	58	48	7.2	1.8	1.3
11283500	1977	9	11	7.6	10	13	21	38	130	81	64	6.6	1.8	1.3
11283500	1977	10	10	7.6	10	15	18	35	103	101	151	6.2	1.8	1.2
11283500	1977	11	9.6	7.8	9.6	13	20	34	97	112	87	5.9	1.8	1.2
11283500	1977	12	9.1	8.2	9.8	14	21	38	105	121	56	5.6	1.7	1.2
11283500	1977	13	8.7	8.6	14	13	22	38	116	124	44	5.2	1.6	1.3
11283500	1977	14	8.4	23	10	12	24	29	110	167	37	5	1.6	1.4
11283500	1977	15	8.3	28	9.5	13	25	36	109	182	33	4.7	1.5	1.4
11283500	1977	16	8.1	18	9.1	13	26	34	126	139	29	4.5	1.5	1.7
11283500	1977	17	8.1	15	8.6	12	28	29	135	118	26	4.1	1.5	2.2
11283500	1977	18	8	17	8.3	14	28	28	118	109	24	3.6	1.5	2.8
11283500	1977	19	8	20	8.2	15	28	30	90	108	22	3.4	1.7	2.8
11283500	1977	20	7.9	19	8.5	16	28	30	72	113	22	3.2	1.8	4.5
11283500	1977	21	7.8	18	8.4	18	78	34	69	140	21	3.2	1.6	5.1
11283500	1977	22	7.8	16	8	20	86	44	69	138	19	3	1.5	4.6
11283500	1977	23	8	15	9.2	23	65	70	68	194	17	2.8	1.4	3.8
11283500	1977	24	8	14	9.5	19	50	67	68	197	16	2.7	1.4	3.3
11283500	1977	25	8.1	14	7.3	18	41	56	64	163	14	2.6	1.4	3.1
11283500	1977	26	8.2	13	8.9	18	40	50	62	134	13	2.5	1.5	2.9
11283500	1977	27	8	12	8.6	18	37	52	60	121	12	2.5	1.6	2.8
11283500	1977	28	8	11	8.1	17	38	59	57	113	11	2.4	1.7	2.8
11283500	1977	29	8	11	9.3	16		53	53	109	10	2.3	1.7	2.9
11283500	1977	30	8	11	11	15		46	48	106	12	2.2	1.6	3.1
11283500	1977	31	8		11	16		38		108		2.1	1.4	
11283500	1978	1	3.2	4.2	14	152	175	376	1290	957	1180	346	47	19
11283500	1978	2	3	4	14	136	171	908	992	1060	1090	357	44	18
11283500	1978	3	2.8	3.9	13	127	167	951	833	1300	1040	300	41	17
11283500	1978	4	2.7	3.9	13	170	165	1920	802	1450	1090	248	39	18
11283500	1978	5	2.7	7.3	13	490	350	2190	707	1380	1160	246	37	51
11283500	1978	6	2.6	13	12	530	600	1450	710	1110	1120	256	35	355
11283500	1978	7	2.6	9	12	310	695	1040	665	1060	1150	271	33	234
11283500	1978	8	2.6	7.1	12	240	680	861	637	1180	1050	244	33	111
11283500	1978	9	2.7	6.6	12	385	1500	769	644	1350	1030	223	33	67
11283500	1978	10	2.7	6.1	12	330	900	702	723	1340	905	230	32	220
11283500	1978	11	2.7	5.8	12	240	725	675	895	1260	728	214	30	150
11283500	1978	12	2.6	5.6	13	200	635	611	1020	1350	816	185	29	81
11283500	1978	13	2.6	5.4	13	190	630	550	1130	1530	864	158	28	59
11283500	1978	14	2.5	5.4	14	350	480	522	1070	1670	846	158	28	53
11283500	1978	15	2.6	5.3	88	420	407	510	1010	1640	756	159	27	70
11283500	1978	16	2.5	5.2	67	455	350	525	876	1130	622	147	26	62
11283500	1978	17	2.4	5.3	200	490	315	582	782	1030	557	130	26	50
11283500	1978	18	2.4	5.4	125	395	290	640	785	1130	598	120	25	43
11283500	1978	19	2.4	5.3	78	400	294	663	794	1160	580	108	25	40
11283500	1978	20	2.5	6.9	60	340	303	706	863	1260	543	99	24	37
11283500	1978	21	2.6	12	59	302	313	849	765	1360	539	93	23	35
11283500	1978	22	2.8	49	180	276	341	990	713	1390	521	87	23	34
11283500	1978	23	2.9	35	495	256	373	842	710	1240	494	82	24	32

11283500	1978	24	2.9	26	270	242	382	761	876	775	491	78	23	30
11283500	1978	25	2.9	21	160	228	369	737	2630	687	439	73	23	29
11283500	1978	26	3	18	132	218	353	814	1810	716	395	73	23	28
11283500	1978	27	3.2	16	375	207	348	862	1450	827	374	72	22	27
11283500	1978	28	3.6	15	295	198	340	942	1340	1100	356	65	22	27
11283500	1978	29	4.2	15	240	191		1020	1150	1250	301	60	21	26
11283500	1978	30	4.2	14	265	184		1530	1120	1290	329	55	19	26
11283500	1978	31	4.4		185	179		1900		1250		50	19	
11283500	1979	1	25	20	84	43	106	260	507	1250	580	88	29	20
11283500	1979	2	25	21	72	44	102	222	499	1080	566	83	28	19
11283500	1979	3	24	22	54	41	93	220	497	1290	545	80	27	18
11283500	1979	4	24	22	52	41	95	231	528	1440	545	78	27	18
11283500	1979	5	23	21	53	48	96	258	646	1540	530	75	26	17
11283500	1979	6	23	21	43	51	98	321	751	1410	510	72	26	17
11283500	1979	7	22	20	34	50	100	425	695	1090	463	69	25	16
11283500	1979	8	22	19	37	81	101	540	732	860	361	65	25	15
11283500	1979	9	21	19	40	95	103	601	810	743	325	62	24	15
11283500	1979	10	21	19	42	81	107	644	717	724	322	58	24	15
11283500	1979	11	23	31	39	1580	110	700	671	794	315	57	23	14
11283500	1979	12	22	27	37	1210	113	701	681	976	308	55	24	14
11283500	1979	13	21	29	36	515	221	698	818	1190	311	53	24	13
11283500	1979	14	20	28	35	349	803	685	922	1310	284	50	24	13
11283500	1979	15	19	26	34	273	464	832	997	1380	226	47	24	13
11283500	1979	16	19	27	33	227	365	749	1020	1350	199	45	23	14
11283500	1979	17	19	28	45	192	288	609	921	1360	187	42	22	16
11283500	1979	18	19	28	67	173	261	544	718	1450	166	40	22	16
11283500	1979	19	19	28	50	148	269	494	638	1440	151	39	21	16
11283500	1979	20	19	33	46	141	263	464	624	1370	157	39	21	16
11283500	1979	21	19	62	48	137	283	436	652	1370	156	44	22	17
11283500	1979	22	19	50	50	131	262	412	696	1280	150	54	22	17
11283500	1979	23	18	44	48	126	237	388	714	1110	146	45	21	17
11283500	1979	24	18	39	48	125	220	398	651	998	141	40	20	18
11283500	1979	25	18	36	49	124	224	441	664	933	133	37	20	18
11283500	1979	26	17	36	50	100	231	498	876	970	124	35	19	18
11283500	1979	27	17	35	52	109	213	744	1650	967	115	34	19	17
11283500	1979	28	17	36	52	104	216	730	1350	870	107	33	18	17
11283500	1979	29	17	38	48	84		617	1300	755	99	32	19	16
11283500	1979	30	18	48	43	106		566	1340	672	93	31	21	16
11283500	1979	31	21		41	105		524		617		30	21	
11283500	1980	1	16	25	67	594	412	645	499	1240	617	446	62	27
11283500	1980	2	16	25	61	321	393	685	471	1300	592	497	59	27
11283500	1980	3	16	34	56	214	377	780	451	1350	580	407	55	26
11283500	1980	4	16	52	52	169	366	790	452	1440	506	360	52	25
11283500	1980	5	16	35	49	145	360	861	569	1370	470	318	51	25
11283500	1980	6	16	30	48	132	369	821	582	1330	472	306	49	24
11283500	1980	7	16	29	51	127	372	725	517	1280	522	278	47	24
11283500	1980	8	16	29	55	126	362	661	500	1140	626	276	45	24
11283500	1980	9	17	29	53	269	347	617	514	1110	707	257	42	25
11283500	1980	10	17	29	53	667	333	599	566	824	726	238	40	25
11283500	1980	11	17	28	50	856	323	586	606	643	688	227	39	25
11283500	1980	12	17	27	42	5100	312	566	623	582	645	217	37	24
11283500	1980	13	17	27	44	9870	301	546	739	592	590	209	35	23
11283500	1980	14	17	27	41	6740	395	537	897	673	511	198	34	23
11283500	1980	15	17	28	40	2620	834	541	892	702	562	190	34	24
11283500	1980	16	17	34	38	2070	1350	525	957	720	611	177	35	24
11283500	1980	17	17	67	36	1770	2890	517	1110	870	626	169	35	23
11283500	1980	18	18	67	36	1370	4520	524	1240	1050	647	164	34	23
11283500	1980	19	21	58	36	1010	4670	508	1270	1200	602	145	33	24
11283500	1980	20	76	46	36	857	2650	516	1320	1330	599	131	34	24
11283500	1980	21	52	42	42	767	2830	509	1110	1360	557	125	32	23
11283500	1980	22	33	44	40	697	1980	486	809	1300	513	117	31	23
11283500	1980	23	28	53	38	643	1450	475	650	1010	467	109	31	22
11283500	1980	24	31	49	107	600	1230	490	624	672	444	102	31	22
11283500	1980	25	28	98	138	571	1010	479	669	569	455	96	32	21
11283500	1980	26	33	172	78	548	870	458	923	515	466	88	31	21
11283500	1980	27	31	121	69	523	745	446	1090	478	422	81	30	20
11283500	1980	28	29	88	67	501	770	451	1280	462	375	76	29	20
11283500	1980	29	28	77	63	484	710	468	1370	462	421	75	28	20
11283500	1980	30	26	72	163	457		498	1330	550	450	70	27	19
11283500	1980	31	25		453	432		517		589		66	27	

11283500	1981	1	19	20	21	26	80	102	293	677	207	23	9.4	6.1
11283500	1981	2	19	20	22	26	82	105	286	619	200	21	9.2	6.2
11283500	1981	3	18	20	24	26	77	100	255	500	171	20	9.1	6.1
11283500	1981	4	18	19	159	35	73	103	239	424	156	20	9.1	6.2
11283500	1981	5	18	19	63	34	72	101	302	399	171	21	9	6.1
11283500	1981	6	18	19	41	28	71	100	383	362	157	22	8.8	6.1
11283500	1981	7	18	19	32	26	69	104	407	346	129	21	8.5	6
11283500	1981	8	18	18	26	26	68	109	377	338	112	20	8.1	6
11283500	1981	9	17	19	28	26	85	117	393	379	100	19	7.8	6
11283500	1981	10	17	19	27	25	84	131	433	402	91	18	7.6	6
11283500	1981	11	18	25	26	25	80	155	400	386	82	18	7.5	6
11283500	1981	12	18	31	27	25	84	147	387	374	74	17	7.4	6
11283500	1981	13	20	26	26	25	87	157	402	369	68	17	7.6	6.3
11283500	1981	14	20	24	26	25	152	132	449	372	63	16	7.6	6.5
11283500	1981	15	23	23	26	25	174	129	479	319	58	16	7.4	6.6
11283500	1981	16	24	22	27	27	165	138	503	272	54	16	7.3	6.6
11283500	1981	17	24	22	27	33	169	137	499	223	51	15	7.1	6.3
11283500	1981	18	24	22	28	31	185	131	493	239	49	14	6.9	6.5
11283500	1981	19	23	22	30	29	183	263	471	509	47	14	6.7	6.7
11283500	1981	20	23	21	29	28	193	306	399	362	44	14	6.8	6.3
11283500	1981	21	22	21	29	28	167	316	392	272	41	13	6.9	6.3
11283500	1981	22	21	21	30	27	159	357	523	242	39	13	6.9	6.3
11283500	1981	23	21	21	32	78	161	339	687	268	36	12	6.8	6.2
11283500	1981	24	20	23	32	67	171	304	769	360	33	12	6.8	6.2
11283500	1981	25	20	22	31	52	144	367	676	337	31	11	6.8	8
11283500	1981	26	24	21	30	49	121	493	640	332	29	11	6.8	11
11283500	1981	27	24	21	29	305	107	378	441	321	27	11	6.6	9.3
11283500	1981	28	23	21	30	341	104	334	474	307	26	10	6.4	8.5
11283500	1981	29	22	21	30	147		346	635	282	24	10	6.2	8.4
11283500	1981	30	21	21	28	100		319	709	273	24	9.7	6	8.3
11283500	1981	31	20		27	85		288		238		9.5	6	
11283500	1982	1	8	63	167	743	298	708	596	1880	557	357	87	30
11283500	1982	2	7.7	64	164	548	297	1040	547	1870	532	288	84	29
11283500	1982	3	9.8	70	158	449	301	738	538	1920	518	264	80	28
11283500	1982	4	13	68	150	443	303	629	604	1960	479	260	80	27
11283500	1982	5	12	65	147	755	286	580	548	1880	445	238	79	26
11283500	1982	6	10	69	141	590	274	546	510	1750	400	221	77	25
11283500	1982	7	12	75	134	467	267	527	471	1750	400	221	76	25
11283500	1982	8	17	67	131	416	261	500	456	1620	406	216	87	24
11283500	1982	9	13	60	133	405	250	499	459	1380	438	206	79	23
11283500	1982	10	14	57	140	395	238	953	1190	1030	457	192	71	22
11283500	1982	11	37	56	132	387	227	1660	10300	871	465	189	67	23
11283500	1982	12	30	65	128	372	220	1170	8140	821	441	184	65	23
11283500	1982	13	21	300	149	349	274	1020	5050	927	403	176	62	22
11283500	1982	14	19	2900	140	339	1540	1200	3180	1060	372	165	60	22
11283500	1982	15	17	470	139	336	5150	1000	2560	1010	407	156	57	24
11283500	1982	16	16	290	133	332	12000	822	2110	1110	426	150	55	49
11283500	1982	17	16	660	121	328	5000	688	1830	1160	436	144	53	45
11283500	1982	18	16	350	117	324	2100	635	1720	1070	434	137	51	44
11283500	1982	19	18	265	1410	321	1500	584	1770	1030	479	133	49	51
11283500	1982	20	21	210	4110	316	1390	546	1810	1120	437	128	47	54
11283500	1982	21	21	180	1840	302	1330	527	1750	1150	374	126	46	43
11283500	1982	22	19	255	837	276	1310	511	1720	1150	332	121	44	37
11283500	1982	23	18	270	603	271	1160	510	1850	1220	327	117	42	34
11283500	1982	24	16	535	494	291	1000	518	1810	1240	323	113	40	63
11283500	1982	25	16	350	442	303	890	539	1690	1170	308	111	38	264
11283500	1982	26	15	260	406	403	760	580	1620	1140	304	106	37	615
11283500	1982	27	15	225	520	408	663	556	1600	1080	298	103	36	164
11283500	1982	28	160	200	460	382	629	617	1810	916	292	101	34	100
11283500	1982	29	130	183	481	339		566	1760	677	350	98	37	79
11283500	1982	30	77	168	961	316		533	1710	600	438	94	34	67
11283500	1982	31	69		717	302		630		600		90	32	
11283500	1983	1	61	293	1000	460	527	3730	1100	1150	2030	1120	184	142
11283500	1983	2	56	224	640	436	489	2880	1110	1060	1640	1130	171	113
11283500	1983	3	52	185	500	417	458	2060	1070	1060	1700	1140	162	84
11283500	1983	4	48	160	465	388	430	1570	978	1140	1760	1160	151	71
11283500	1983	5	46	144	430	370	414	1350	905	1070	1910	1110	140	64
11283500	1983	6	44	133	395	353	474	1200	828	993	2110	1020	134	60
11283500	1983	7	48	125	360	334	1330	1300	786	963	2190	932	131	56
11283500	1983	8	47	123	330	327	1580	1200	784	955	2010	755	124	53

11283500	1983	9	44	128	308	312	1040	1140	815	970	2000	699	121	52
11283500	1983	10	42	144	290	304	837	1120	826	925	2120	544	117	51
11283500	1983	11	40	131	281	299	718	1340	766	880	2300	584	113	49
11283500	1983	12	39	139	278	303	795	1330	717	905	1940	594	107	46
11283500	1983	13	38	131	293	302	1470	4360	674	900	1770	600	97	45
11283500	1983	14	37	135	273	298	1080	2740	634	895	1830	584	99	44
11283500	1983	15	36	134	260	292	937	1830	615	980	1940	556	112	42
11283500	1983	16	35	130	249	311	817	1520	624	1060	2010	467	98	41
11283500	1983	17	34	128	272	301	739	1390	670	1220	2030	425	84	40
11283500	1983	18	34	935	280	318	822	1260	709	1490	1990	405	80	39
11283500	1983	19	34	929	282	338	767	1130	750	1770	1700	387	83	38
11283500	1983	20	33	441	660	301	724	1080	928	2080	1530	361	84	37
11283500	1983	21	34	324	2000	291	672	1080	899	2390	1400	331	81	37
11283500	1983	22	39	386	4400	803	645	1010	909	2600	1490	336	78	38
11283500	1983	23	56	421	3000	772	660	966	1040	2730	1580	328	76	43
11283500	1983	24	123	327	1300	1770	671	962	1060	2930	1470	303	73	45
11283500	1983	25	1490	290	910	1070	712	913	968	3080	1420	310	69	43
11283500	1983	26	2260	267	790	817	875	841	886	3170	1400	262	66	41
11283500	1983	27	445	259	695	1150	995	898	848	3220	1360	248	62	40
11283500	1983	28	269	310	630	857	1390	937	1130	3170	1320	235	60	40
11283500	1983	29	204	700	582	786	843	1300	3230	1250	219	58	47	
11283500	1983	30	774	1990	535	657	853	1300	2770	1170	209	56	175	
11283500	1983	31	477		494	585		1110		2610		200	62	
11283500	1987	1	30	20	19	23	30	49	202	312	59	13	6.3	5.1
11283500	1987	2	27	20	20	25	29	51	233	191	54	13	6.1	5.3
11283500	1987	3	25	20	21	40	32	52	283	172	50	13	5.9	5.5
11283500	1987	4	25	19	20	72	30	58	213	197	45	13	5.7	5.4
11283500	1987	5	26	19	21	40	28	283	185	213	41	12	5.5	5.5
11283500	1987	6	26	19	25	34	28	435	211	216	40	12	5.3	5.6
11283500	1987	7	26	19	27	33	30	267	258	192	44	12	5.1	5.8
11283500	1987	8	25	20	23	25	31	195	301	179	56	11	5	5.7
11283500	1987	9	25	20	19	21	32	169	306	282	49	11	4.9	5.4
11283500	1987	10	25	20	18	23	44	148	335	288	40	11	4.9	5.2
11283500	1987	11	24	20	19	25	63	129	342	228	35	10	4.8	5
11283500	1987	12	24	20	21	21	76	127	312	197	31	10	4.8	5
11283500	1987	13	24	19	22	27	524	244	286	174	28	9.7	4.9	5.1
11283500	1987	14	23	19	21	21	231	215	321	154	26	9.3	4.9	5.3
11283500	1987	15	23	19	20	21	135	187	330	139	25	8.7	5	5.4
11283500	1987	16	23	19	20	16	98	167	326	260	26	8	5.3	5.2
11283500	1987	17	22	19	21	23	90	168	340	195	25	7.6	5.3	5
11283500	1987	18	22	19	22	27	77	192	328	140	23	8.3	5	4.9
11283500	1987	19	22	19	23	24	65	173	203	116	22	8.9	4.8	4.8
11283500	1987	20	22	20	24	22	64	142	201	103	21	8.8	4.8	4.6
11283500	1987	21	23	20	22	22	57	143	247	139	20	8.8	4.8	4.5
11283500	1987	22	23	20	20	23	56	133	286	144	19	9.1	4.8	4.5
11283500	1987	23	22	20	23	25	57	142	270	124	19	9.1	4.8	4.3
11283500	1987	24	22	20	22	29	48	128	269	105	18	8.7	4.7	4.3
11283500	1987	25	22	20	20	35	52	134	269	89	17	8.5	4.8	4.4
11283500	1987	26	21	19	21	30	43	138	288	81	16	8.1	4.7	4.5
11283500	1987	27	21	19	23	30	47	150	344	79	15	7.7	4.6	4.7
11283500	1987	28	21	19	19	40	48	153	292	72	14	7.3	4.4	4.7
11283500	1987	29	21	19	20	37		155	287	67	14	6.9	4.4	4.6
11283500	1987	30	21	21	19	33		173	396	65	14	6.6	4.4	4.5
11283500	1987	31	21		21	31		201		62		6.5	4.9	
11283500	1988	1	4.4	17	19	36	80	290	169	226	119	21	6.2	2.8
11283500	1988	2	4.4	15	22	37	73	210	185	199	109	19	5.4	2.9
11283500	1988	3	4.3	14	21	72	66	220	222	186	104	18	5.1	2.8
11283500	1988	4	4.4	16	22	97	66	210	170	189	98	17	4.9	2.7
11283500	1988	5	4.4	15	23	209	63	230	190	174	89	16	4.9	2.6
11283500	1988	6	4.3	18	37	161	67	230	210	167	78	16	4.8	2.7
11283500	1988	7	4.4	20	91	123	70	220	222	157	85	15	4.7	2.6
11283500	1988	8	4.5	24	56	101	74	230	220	158	89	15	4.7	2.6
11283500	1988	9	4.6	20	50	89	91	240	190	162	85	14	4.5	2.6
11283500	1988	10	4.9	17	70	86	104	210	200	164	78	13	4.4	2.7
11283500	1988	11	5	15	89	108	113	170	220	205	70	13	4.1	2.7
11283500	1988	12	5.2	14	63	86	120	150	210	257	65	12	4	2.8
11283500	1988	13	5.4	17	38	75	123	140	200	252	60	11	4	2.8
11283500	1988	14	6	31	29	67	120	150	240	235	56	11	4	2.8
11283500	1988	15	5.9	29	37	71	128	160	230	230	50	11	4.1	2.9
11283500	1988	16	5.8	24	36	71	134	150	220	234	47	11	4.1	3

11283500	1988	17	5.6	24	33	88	117	160	200	349	44	10	4.1	3
11283500	1988	18	5.5	42	28	79	109	179	180	254	41	9.3	3.9	3
11283500	1988	19	5.4	37	29	63	97	203	200	196	38	8.4	3.7	3
11283500	1988	20	5.3	33	25	66	102	215	210	183	38	7.7	3.5	3.2
11283500	1988	21	5.3	33	26	63	119	218	200	182	39	7.4	3.4	3.3
11283500	1988	22	5.6	31	54	61	131	196	200	174	36	7.2	3.3	3.6
11283500	1988	23	14	32	59	66	151	220	170	157	32	6.8	3.3	3.8
11283500	1988	24	14	27	50	80	160	253	200	148	31	6.7	3.3	3.9
11283500	1988	25	13	24	40	99	175	251	250	134	29	18	3.2	3.8
11283500	1988	26	11	21	44	107	198	276	400	125	30	27	3.1	3.8
11283500	1988	27	9.3	18	39	102	213	283	350	109	27	18	3	3.9
11283500	1988	28	15	18	43	98	277	236	320	102	25	12	3	3.9
11283500	1988	29	34	18	40	98	295	198	315	185	24	9.5	2.9	3.8
11283500	1988	30	39	17	39	96		195	287	165	22	8	2.9	3.6
11283500	1988	31			31	87		176		140		7	2.8	

APPENDIX G
Flow Records for
Clavey River Gage #11283500
From Turlock Irrigation District Files

DAY	OCT	NOV	DEC	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP
1	30	20	19	23	30	49	202	312	59	13	6.3	5.1
2	27	20	20	25	29	51	233	191	54	13	6.1	5.3
3	25	20	21	40	32	52	283	172	50	13	5.9	5.5
4	25	19	20	72	30	58	213	197	45	13	5.7	5.4
5	26	19	21	40	28	283	185	213	41	12	5.5	5.5
6	26	19	25	34	28	435	211	216	40	12	5.3	5.6
7	26	19	27	33	30	267	258	192	44	12	5.1	5.8
8	25	20	23	25	31	195	301	179	56	11	5	5.7
9	25	20	19	21	32	169	306	282	49	11	4.9	5.4
10	25	20	18	23	44	148	335	288	40	11	4.9	5.2
11	24	20	19	25	63	129	342	228	35	10	4.8	5
12	24	20	21	21	76	127	312	197	31	10	4.8	5
13	24	19	22	27	524	244	286	174	28	9.7	4.9	5.1
14	23	19	21	21	231	215	321	154	26	9.3	4.9	5.3
15	23	19	20	21	135	187	330	139	25	8.7	5	5.4
16	23	19	20	16	98	167	326	260	26	8	5.3	5.2
17	22	19	21	23	90	168	340	195	25	7.6	5.3	5
18	22	19	22	27	77	192	328	140	23	8.3	5	4.9
19	22	19	23	24	65	173	203	116	22	8.9	4.8	4.8
20	22	20	24	22	64	142	201	103	21	8.8	4.8	4.6
21	23	20	22	22	57	143	247	139	20	8.8	4.8	4.5
22	23	20	23	23	56	133	286	144	19	9.1	4.8	4.5
23	22	20	23	25	57	142	270	124	19	9.1	4.8	4.3
24	22	20	22	29	48	128	269	105	18	8.7	4.7	4.3
25	22	20	20	35	52	134	269	89	17	8.5	4.8	4.4
26	21	19	21	30	43	138	288	81	16	8.1	4.7	4.5
27	21	19	23	30	47	150	344	79	15	7.7	4.6	4.7
28	21	19	19	40	48	153	292	72	14	7.3	4.4	4.7
29	21	19	20	37	—	155	287	67	14	6.9	4.4	4.6
30	21	21	19	33	—	173	396	65	14	6.6	4.4	4.5
31	21	—	—	21	31	—	201	—	62	—	6.5	4.9
TOTAL	727	586	656	898	2145	5101	8484	4975	906	297.6	155.6	149.8
MEAN	23.5	19.5	21.2	29	76.6	165	282	160	30.2	9.6	5.02	4.99
MAX	30	21	27	72	524	435	396	312	59	13	6.3	5.8
MIN	21	19	18	16	28	49	185	62	14	6.5	4.4	4.3
AC-FT	1440	1160	1300	1780	4250	10120	16790	9870	1800	590	309	297

More? [Y/N DEF AULT=Y]:
 H0 1;1H 2J0 [1;1H U. S. DEPAR'MENT OF THE INTERIOR - U.S. GEOLOGICAL SURVEY #NAME? RESOURCES

STATIO N NUMBER 11283500 CLAVEY RNR BUCK MEADOWS CA SOU CE AGEN USGS STATE 06 COUNTY 1 9
 LATIT UDE 375 402 LONGITUDE 12 00415 NA D27 DRAI NAGE AREA 144* CO NTRIBUTI G DRAINAGE AREA DATUM 2374.08 NG VD29
 Date Processed: 2006-11-21 09:19 By turloc k
 Lowes Tagging status in period is APPROVED
 DD #1

D Ischarge, cubic feet per second
 WATER YEAR OCTOBER 1987 TO SEPTEMBER 1988
 DA ILY MEAN VALUES

DAY	OCT	NOV	DEC	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP
1	4.4	17	19	36	80	290	169	226	119	21	6.2	2.8
2	4.4	15	22	37	73	210	185	199	109	19	5.4	2.9
3	4.3	14	21	72	66	220	222	186	104	18	5.1	2.8
4	4.4	16	22	97	66	210	170	189	98	17	4.9	2.7
5	4.4	15	23	209	63	230	190	174	89	16	4.9	2.6
6	4.3	18	37	161	67	230	210	167	78	16	4.8	2.7
7	4.4	20	91	123	70	220	222	157	85	15	4.7	2.6
8	4.5	24	56	101	74	230	220	158	89	15	4.7	2.6
9	4.6	20	50	89	91	240	190	162	85	14	4.5	2.6
10	4.9	17	70	86	104	210	200	164	78	13	4.4	2.7
11	5	15	89	108	113	170	220	205	70	13	4.1	2.7
12	5.2	14	63	86	120	150	210	257	65	12	4	2.8
13	5.4	17	38	75	123	140	200	252	60	11	4	2.8
14	6	31	29	67	120	150	240	235	56	11	4	2.8
15	5.9	29	37	71	128	160	230	230	50	11	4.1	2.9
16	5.8	24	36	71	134	150	220	234	47	11	4.1	3
17	5.6	24	33	88	117	160	200	349	44	10	4.1	3

18	5.5	42	28	79	109	179	180	254	41	9.3	3.9	3
19	5.4	37	29	63	97	203	200	196	38	8.4	3.7	3
20	5.3	33	25	66	102	215	210	183	38	7.7	3.5	3.2
21	5.3	33	26	63	119	218	200	182	39	7.4	3.4	3.3
22	5.6	31	54	61	131	196	200	174	36	7.2	3.3	3.6
23	14	32	59	66	151	220	170	157	32	6.8	3.3	3.8
24	14	27	50	80	160	253	200	148	31	6.7	3.3	3.9
25	13	24	40	99	175	251	250	134	29	18	3.2	3.8
26	11	21	44	107	198	276	400	125	30	27	3.1	3.8
27	9.3	18	39	102	213	283	350	109	27	18	3	3.9
28	15	18	43	98	277	236	320	102	25	12	3	3.9
29	34	18	40	98	295	198	315	185	24	9.5	2.9	3.8
30	39	17	39	96 ---		195	287	165	22	8	2.9	3.6
31	23 ---		31	87 ---		176 ---		140 ---		7	2.8 ---	

TOTAL	282.9	681	1283	2742	3636	6469	6780	5798	1738	396	123.3	93.6
MEAN	9.13	22.7	41.4	88.5	125	209	226	187	57.9	12.8	3.98	3.12
MAX	39	42	91	209	295	290	400	349	119	27	6.2	3.9
MIN	4.3	14	19	36	63	140	169	102	22	6.7	2.8	2.6
AC-FT	561	1350	2540	5440	7210	12830	13450	11500	3450	785	245	186

More? [YN DEF AULT=Y]; U. S. DEPARTMENT OF THE INTERIOR - U.S. GEOLOGICAL SURVEY NAME? RESOURCES

LATIT STATION NUMBER: 11283500 CLAVEY RNR BUCK MEADOWS CA SOURCE: AGENT/USGS STATE: 06 COUNTY: 1 9
UDE 375 402 LONGITUDE: 1200415 NA D27 DRAI NAGE AREA: 144* CO NTRIBUTI G DRAINAGE AREA: DATUM: 2374.08 NGVD29

EATN UDE 373 402 LONGITUDE 12 00415 NA 27° DRA NAGE AREA 144 °C NITROBOTTIG DRANA LAKER DATUM 23/74.00 NG VB25
 Date Processed: 2006-11-21 09:19 By turloc k
 Lowes aging status in period is APPROVED
 DD #1
 Discharge, cubic feet per second
 WATER YEAR OCTOBER 1988 TO SEPTEMBER 1989
 DA ILY MEAN VALUES

DAY	OCT	NOV	DEC	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP
1	3.4	4.4	46	50	133	197	685	341	141	33	8.4	5.4
2	3.4	4.5	43	50	116	367	570	355	146	30	8.3	5.4
3	3.3	4.6	45	50	95	285	580	359	149	28	8.2	5.3
4	3.3	4.8	40	53	71	217	614	426	162	26	8	5.3
5	3.3	4.9	37	62	71	206	732	443	149	24	7.8	5.1
6	3.4	4.9	40	55	82	387	826	457	137	22	7.8	4.9
7	3.6	4.8	42	59	85	747	875	419	170	21	7.6	4.8
8	3.8	4.9	45	56	79	2400	859	410	168	19	8.6	4.8
9	3.9	5.3	43	56	109	1390	872	411	189	18	9.9	4.9
10	3.8	5.6	39	59	135	1080	842	495	154	17	9.8	4.9
11	3.8	6	38	59	116	1150	747	344	139	16	8.7	4.9
12	3.8	6.4	41	55	101	852	712	310	131	16	7.9	4.9
13	3.9	14	42	54	95	660	624	268	123	16	7.4	4.8
14	4.2	44	45	52	89	516	652	277	113	15	7.1	4.7
15	4.2	24	41	49	84	468	624	325	100	14	6.8	4.7
16	4.3	17	33	49	85	479	593	297	94	14	6.5	5.1
17	4.3	32	40	49	89	409	536	289	89	14	6.3	36
18	4.1	20	37	53	99	396	550	301	77	13	6.3	35
19	4	14	34	58	123	562	493	254	68	13	6.4	40
20	4	13	40	68	127	622	554	249	62	13	6.4	27
21	4	12	45	77	120	521	605	246	57	12	6.4	22
22	4	13	40	77	143	545	447	236	52	11	6.3	16
23	4	125	39	77	222	573	366	228	48	11	6.1	14
24	4	82	58	71	306	880	347	185	45	10	6.1	12
25	4	69	56	62	233	1140	320	162	43	10	6.1	11
26	4	59	46	63	235	714	295	175	44	9.6	6	10
27	4	48	47	60	271	606	274	187	42	9.2	5.9	9.5
28	4	45	51	61	229	1060	287	184	40	9	5.7	9.2
29	4.1	46	50	66 ---		1060	303	160	36	8.7	5.5	17

TOTAL	120.6	783.1	1343	1883	3743	21986	17113	9067	3002	489.4	218.9	437.6
MEAN	3.89	26.1	43.3	60.7	134	709	570	292	100	15.8	7.06	14.6
MAX	4.4	125	58	100	306	2400	875	495	189	33	9.9	99
MIN	3.3	4.4	33	49	71	197	274	131	34	8.4	5.3	4.7
AC-FT	239	1550	2660	3730	7420	43610	33940	17980	5950	971	434	868

D[H0] 2J0[1;1H D[1;1H U. S. DEPARTMENT OF THE INTERIOR - U.S. GEOLOGICAL SURVEY #NAME? RESOURCES

LATIT STATION NUMBER 11283500 CLAVEY RNR BUCK MEADOWS CA SOURCE AGENT USGS STATE 06 COUNTY 1 9
 UDE 375 402 LONGITUDE 12 00415 NA D27 DRAINAGE AREA 144* CO NTRIBUTI G DRAINA E AREA DATUM 2374.08 NG VD29

Date Processed: 2006-11-21 09:19 By turloc k
 Lowes taging s tatus in period is APPROVED
 DD #1

D ischarge, cubic fe et per se cond
 WATER YEAR OCTOBER 1989 TO SEPTEMBER 1990
 DA ILY MEAN VALUES

DAY	OCT	NOV	DEC	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP
1	45	69	56	28	64	201	326	192	195	23	7	4.1
2	28	64	55	32	58	190	351	189	159	21	6.7	4.1
3	21	59	58	26	62	264	362	196	142	20	6.5	4
4	18	56	60	28	67	293	381	201	127	20	6.3	3.8
5	16	58	66	29	62	228	349	206	116	19	6.1	3.6
6	15	57	68	29	72	207	357	204	108	18	5.7	3.6
7	14	51	64	33	60	203	354	187	100	18	5.6	3.6
8	13	46	59	47	53	214	365	168	92	18	5.5	3.4
9	12	42	55	68	65	227	315	157	85	17	5.5	3.2
10	12	40	50	59	63	245	318	153	79	16	5.7	3.1
11	11	40	44	53	71	218	353	134	71	15	5.4	3
12	11	41	43	52	84	190	356	124	64	17	5.1	2.9
13	10	40	44	130	84	169	368	120	58	15	4.8	2.8
14	10	37	40	124	63	167	407	116	56 e14	4.6	2.8	
15	10	34	41	101	62	169	394	108	57 e13	4.6	2.8	
16	10	32	39	92	76	191	398	102	59 e20	4.5	2.9	
17	10	30	36	69	51	211	302	100	52 e14	4.6	3	
18	10	29	35	74	61	269	250	93	47 e13	4.6	3.1	
19	9.8	28	34	65	72	312	289	86	44 e12	4.7	3.3	
20	9.6	27	33	60	75	337	285	81	41 e11	5.2	3.4	
21	10	26	36	59	72	371	304	75	38 e11	5.4	3.6	
22	30	26	33	62	74	382	263	70	35 e10	5.3	3.9	
23	156	25	34	61	87	376	394	88	33 e9.6	5.1	4.6	
24	871	29	33	59	103	394	399	137	31 e9.4	4.9	4.9	
25	311	46	31	61	117	415	320	155	30 e9.0	4.6	6.4	
26	167	156	31	62	128	400	319	129	28	8.7	4.6	7.4
27	130	71	32	58	150	382	323	151	27	8.6	4.7	6.4
28	114	70	29	55	180	364	327	424	25	8.4	4.8	6.1
29	96	63	28	56 --		317	302	307	25	8	4.6	7.1
30	84	59	26	61 --		304	228	200	24	7.7	4.3	6.3
31	75 --		30	61 --		306 --		227 --		7.4	4.1 --	
TOTAL	2339.4	1451	1323	1854	2236	8516	10059	4880	2048	431.8	161.1	123.2
MEAN	75.5	48.4	42.7	59.8	79.9	275	335	157	68.3	13.9	5.2	4.11
MAX	871	156	68	130	180	415	407	424	195	23	7	7.4
MIN	9.6	25	26	26	51	167	228	70	24	7.4	4.1	2.8
AC-FT	4640	2880	2620	3680	4440	16890	19950	9680	4060	856	320	244

e Estimate d
 More? [Y/N DEF AULT=Y]:
 D[H0] 2J0[1;1H D[1;1H U. S. DEPARTMENT OF THE INTERIOR - U.S. GEOLOGICAL SURVEY #NAME? RESOURCES

LATIT STATION NUMBER 11283500 CLAVEY RNR BUCK MEADOWS CA SOURCE AGENT USGS STATE 06 COUNTY 1 9
 UDE 375 402 LONGITUDE 12 00415 NA D27 DRAINAGE AREA 144* CO NTRIBUTI G DRAINA E AREA DATUM 2374.08 NG VD29

Date Processed: 2006-11-21 09:19 By turloc k
 Lowes taging s tatus in period is APPROVED
 DD #1

D ischarge, cubic fe et per se cond
 WATER YEAR OCTOBER 1990 TO SEPTEMBER 1991
 DA ILY MEAN VALUES

DAY	OCT	NOV	DEC	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP
1	5.2	8.2	8.4	9.1	10	109	321	644	434	125	12	5.7
2	4.9	9.9	7.9	9.4	11	69	283	452	506	96	12	5.6
3	4.7	8.5	7.7	10	14	138	296	374	505 e78	12	5.5	
4	4.7	7.7	7.8	14	13	824	388	367	487 e63	11	5.2	
5	4.5	7.3	7.7	14	28	882	494	498	449 e54	11	5	
6	4.3	6.7	7.7	13	24	340	530	692	386 e54	11	4.8	
7	4.3	6.4	7.6	12	17	207	480	803	344 e49	11	5.2	

8	4.4	6.4	7.4	13	15	165	446	923	334 e45	11	5.2
9	4.5	6.5	7.4	12	14	162	464	767	332 e41	10	5.4
10	4.5	6.5	7.4	12	14	147	482	497	317 e37	9.7	5.1
11	4.5	6.4	7.7	11	14	120	378	439	298 e34	9.3	5.1
12	4.5	6.3	8.8	11	14	115	328	386	273 e32	9.1	5.2
13	4.4	6.2	9.4	12	13	122	351	494	252 e29	9.1	5.3
14	4.5	6.2	9	13	13	107	433	454	213 e27	9.3	5.1
15	4.5	6.2	9.1	12	14	105	469	528	181 e27	9.2	4.9
16	4.5	6.2	9.3	12	15	95	390	671	161	26	9.5
17	4.5	6.2	9.1	11	16	105	352	641	144	25	9.3
18	4.6	6.2	9.7	11	17	108	348	461	129	24	8.8
19	5.2	6.6	11	11	14	129	372	386	117	24	8.4
20	5.7	9.8	9.6	10	14	127	392	399	105	24	7.9
21	5.7	10	9.2	10	14	108	398	418	94	27	7.5
22	5.7	8.9 e8.4		9.3	14	95	422	535	87	25	7.1
23	5.6	8.3 e8.5		9.5	14	105	439	669	79	22	6.8
24	5.4	7.9	8.8	10	13	148	497	740	73	20	6.6
25	5.3	8	9	9.8	13	189	455	730	69	18	6.3
26	5	11	9.1	9.3	14	128	385	651	65	18	6
27	4.9	9.5	9.3	9.4	14	119	418	538	62	17	6
28	4.8	8.5	9.6	9	32	148	465	492	102	16	6.1
29	4.9	8.5	9.3	8.6 ---		161	567	506	342	15	6.3
30	4.9	8.5	8.9	9.1 ---		197	648	486	196	14	6.2
31	5.6 ---		8.9	9.7 ---		261 ---		421 ---		13	6 ---
TOTAL	150.7	229.5	268.7	336.2	432	5836	12691	17062	7136	1119	271.5
MEAN	4.86	7.65	8.67	10.8	15.4	188	423	550	238	36.1	8.76
MAX	5.7	11	11	14	32	882	648	923	506	125	5.7
MIN	4.3	6.2	7.4	8.6	10	69	283	367	62	13	3.9
AC-FT	299	455	533	667	857	11580	25170	33840	14150	2220	539

STATISTICS OF MONTHLY MEAN DATA FOR WATER YEARS 1960 - 1991, BY WATER YEAR (WY)

MEAN	28.5	78	159	276	326	421	608	706	344	86.7	24	18.1
MAX	226	339	999	1331	1426	1482	2057	1754	1746	566	101	69.4
(WY)	1983	1983	1965	1980	1982	1983	1982	1983	1983	1983	1983	1982
MIN	2.89	7.65	8.67	10.8	15.4	39	84.4	117	30.2	5.06	1.66	2.28
(WY)	1978	1991	1991	1991	1991	1977	1977	1977	1987	1977	1977	1977

SUMMA	RY	STATI	STICS	FO	R 1990 CALENDAR YAR	FOR 1991 WATER YAR	WATER Y EARS 1960	-1991
ANNUA	L	TOTAL		30958	0	45673	0.8	
ANNUA	L	MEAN		84	0.8	125		256
HIGHE	ST	ANNUAL MEAN					771	1983
LOWES	T	ANNUAL MEAN					31	0
HIGHE	ST	DAILY MEAN		424 May	28	923 May	8	12000 Feb 16 1982
LOWES	T	DAILY MEAN		2.8 Sep	13	3.9 Sep	27	1.2 Sep 10 1977
ANNUA	L	SEVEN- DAY MINIMUM		2.9 Sep	11	4.0 Sep	24	1.3 Sep 7 1977
MAXIM	UM	PEAK FLOW					19400 Jan	13 1980
MAXIM	UM	PEAK STAGE					21.47 Jan	13 1980
ANNUA	L	RUNOFF (AC-FT)		61410		90590		185300
10 PE	RCENT	ECEEDS		305		457		668
50 PE	RCENT	ECEEDS		21		13		74
90 PE	RCENT	ECEEDS		4	0.5	4	0.9	9 0

e Estimate d
More? [Y/N DEF AULT=Y]:
D[1;H] D[1;1H] U. S. DEPARTMENT OF THE INTERIOR - U.S. GEOLOGICAL SURVEY NAME? RESOURCES

STATION NUMBER 11283500 CLAVEY RNR BUCK MEADOWS CA SOURCE AGENCY USGS STATE 06 COUNTY 1 9
LATIT UDE 375 402 LONGITUDE 1200415 NA D27 DRA NAGE AREA 144 CO NTRIBUTING DRAINAGE AREA DATUM 2374.08 NGVD29

Date Processed: 2006-11-21 09:19 By turloc k
Lowes taging s status in period is APPROVED

DD #1

Discharge, cubic feet per second
WATER YEAR OCTOBER 1991 TO SEPTEMBER 1992
DAI LY MEAN VALUES

DAY	OCT	NOV	DEC	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP
1	4	20	23	31	36	261	440	284	46	86	12	6.4
2	4	22	25	30	34	237	471	241	39	46	11	6.5
3	4	25	23	31	31	304	523	227	35	33	10	7.4
4	4	28	22	30	34	286	541	226	32	27	9.8	6.9

5	3.9	29	21	43	33	275	486	217	30	23	9.2	6.5
6	3.9	31	21	41	32	333	411	232	28	21	9	6.1
7	3.8	33	23	43	40	277	396	268	28	19	8.7	5.6
8	3.8	31	24	39	59	253	414	250	31	17	8.5	5.2
9	3.8	29	22	38	64	234	408	236	29	16	8.3	5
10	3.8	34	22	38	87	232	390	181	26	15	8.1	4.7
11	3.8	32	22	35	135	249	394	162	24	14	7.7	4.5
12	3.8	26	21	33	250	281	372	155	23	235	7.2	4.4
13	3.8	22	20	37	257	301	575	144	23	173	6.8	4.3
14	3.8	20	20	35	173	327	499	140	24	108	6.8	4.3
15	3.8	18	20	34	178	320	430	128	24	96	12	4.2
16	3.8	17	18	35	148	293	366	117	28	74	26	4.1
17	3.8	22	19	36	135	254	474	111	28	135	15	3.9
18	3.8	53	27	36	129	235	507	103	25	78	11	3.9
19	3.8	34	36	35	125	228	401	95	22	48	8.7	3.9
20	3.8	30	23	34	281	220	417	88	21	36	7.4	3.9
21	3.8	37	23	36	329	221	432	76	20	30	6.6	3.9
22	3.8	58	25	32	325	243	369	68	21	27	6.1	3.9
23	3.8	50	24	33	337	254	302	63	18	24	5.8	3.7
24	4.1	39	22	34	275	241	303	60	18	22	5.7	3.6
25	4.7	37	21	36	270	250	329	57	21	21	5.6	3.4
26	165	36	22	35	293	306	358	56	22	19	5.5	3.5
27	98	36	21	35	299	313	357	53	19	17	5.3	3.4
28	39	34	36	305	384	345	72	17	16	5.2	3.4	
29	28	29	51	35	281	390	369	63	18	15	4.9	3.3
30	25	23	41	36 ---	413	372	52	71	13	4.7	3.3	
31	23 ---		34	36 ---	390 ---		47 ---		12	5.3 ---		
TOTAL	475.2	935	770	1098	4975	8805	12451	4272	811	1516	263.9	137.1
MEAN	15.3	31.2	24.8	35.4	172	284	415	138	27	48.9	8.51	4.57
MAX	165	58	51	43	337	413	575	284	71	235	26	7.4
MIN	3.8	17	18	30	31	220	302	47	17	12	4.7	3.3
AC-FT	943	1850	1530	2180	9870	17460	24700	8470	1610	3010	523	272

STATISTICS OF MONTHLY MEAN DATA FOR WATER YEARS 1960 - 1992, BY WATER YEAR (WY)

MEAN	28.1	76.4	155	268	320	417	602	687	334	86.4	23.5	17.6
MAX	226	339	999	1331	1426	1462	2057	1754	1746	566	101	69.4
(WY)	1983	1983	1965	1980	1982	1983	1982	1983	1983	1983	1983	1982
MIN	2.89	7.65	8.67	10.8	15.4	39	84.4	117	27	5.06	1.66	2.28
(WY)	1978	1991	1991	1991	1991	1977	1977	1977	1992	1977	1977	1977

SUMMA	RY	STATISTICS	FO	R 1991 CALENDAR YEAR	FOR 1992 WATER YEAR				WATER YEARS 1960 - 1992			
ANNUAL	L TOTAL		47205	0.1		36509	0.2					
ANNUAL	L MEAN		129			99	0.8		251			
HIGHEST	ST ANNUAL MEAN								771			1983
LOWEST	ST ANNUAL MEAN								31	0		1977
HIGHEST	ST DAILY MEAN			923 May		8	575 Apr		13	12000 Feb		16 1982
LOWEST	ST DAILY MEAN			3.8 Oct		7	3.3 Sep		29	1.2 Sep		10 1977
ANNUAL	L SEVEN-DAY MINIMUM			3.8 Oct		7	3.4 Sep		24	1.3 Sep		7 1977
MAXIMUM	UM PEAK FLOW					727 Apr		13	19400 Jan			13 1980
MAXIMUM	UM PEAK STAGE					7.34 Apr		13	21.47 Jan			13 1980
ANNUAL	L RUNOFF (AC-FT)		93630			72420			181500			
10 PERCENT	RECENT EXCEEDS		457			326			648			
50 PERCENT	RECENT EXCEEDS		24			32			71			
90 PERCENT	RECENT EXCEEDS		4	0.4		4	0		8	0.7		

More? [Y/N DEF AULT=Y]:
 HOD [2J0[1;1H 1;1H U. S. DEPARTMENT OF THE INTERIOR - U.S. GEOLOGICAL SURVEY #NAME? RESOURCES

STATION NUMBER 11283500 CLAVEY RNR BUCK MEADOWS CA SOURCE AGENT USGS STATE 06 COUNTY 1 9
LATIT UDE 375 402 LONGITUDE 1200415 NA D27 DRAINAGE AREA 144* CO NTRIBUTING DRAINAGE AREA DATUM 2374.08 NGVD29
Date Processed: 2006-11-21 09:19 By turloc k
Lowest Tagging Status in period is APPROVED
DD#1
D WATER ischarge, cubic feet per second
YEAR OCTOBER 1992 TO SEPTEMBER 1993
DA ILY MEAN VALUES

DAY	OCT	NOV	DEC	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP
1	3.2	40	13	68	253	305	1320	1490	860	262	38	15
2	3.3	48	14	66	240	303	1090	1460	670	262	36	14

3	3.3	57	13	54	235	320	1030	1370	582	252	34	14
4	3.5	47	13	53	224	337	1100	1050	635	214	33	14
5	3.6	36	12	53	267	352	1040	989	873	213	31	14
6	3.7	32	15	58	313	393	843	1090	600	212	29	14
7	3.7	29	92	527	303	443	791	1040	560	208	27	14
8	3.7	28	35	527	443	490	882	1050	615	194	26	13
9	3.7	24	302	349	551	523	997	1120	569	175	25	13
10	3.6	21	120	254	449	528	1020	1310	624	158	25	12
11	3.6	18	185	184	421	538	966	1420	656	146	24	12
12	3.6	17	91	164	385	564	909	1330	614	136	24	12
13	3.6	15	60	724	351	619	819	842	594	125	23	12
14	3.6	15	54	963	328	828	772	897	639	116	23	12
15	3.6	14	48	535	305	850	848	977	638	105	23	12
16	3.7	14	42	704	286	699	933	990	572	94	22	12
17	3.8	13	46	566	284	2000	846	1170	500	83	22	12
18	3.9	13	39	490	356	1770	940	1230	507	78	21	13
19	4	13	35	367	707	1260	804	1230	507	74	20	14
20	4	13	41	436	594	1090	851	1220	510	71	20	13
21	4.6	13	37	1170	487	1090	1060	1130	456	68	20	13
22	6.7	13	35	1870	430	1160	1210	964	379	64	19	13
23	7	15	35	887	458	1220	1170	986	366	61	18	12
24	6.2	18	36	602	459	1910	843	1050	372	61	18	12
25	5.7	17	36	471	390	1800	890	1490	386	58	17	12
26	5.6	16	38	404	365	1650	997	1060	380	55	17	12
27	5.3	15	37	369	336	1250	1150	846	357	53	16	12
28	5.3	15	50	343	318	1020	1230	692	335	50	16	11
29	25	15	146	320 ---		872	1390	617	284	47	15	11
30	77	14	89	299 ---		881	1530	693	258	44	15	11
31	77 ---		68	274 ---		908 ---		1040 ---	41	15 ---		

TOTAL 298.1 658 1877 14151 10538 27973 30271 33843 15898 3780 712 380
 MEAN 9.62 21.9 60.5 456 376 902 1009 1092 530 122 23 12.7
 MAX 77 57 302 1870 707 2000 1530 1490 873 262 38 15
 MIN 3.2 13 12 53 224 303 772 617 258 41 15 11
 AC-FT 591 1310 3720 28070 20900 55480 60040 67130 31530 7500 1410 754

STATISTICS OF MONTHLY MEAN DATA FOR WATERSHED YEARS 1960 - 1993, BY WATER YEAR (WY)

MEAN	27.5	74.7	152	274	322	433	615	700	340	86.6	23.5	17.5
MAX	226	339	999	1331	1426	1482	2057	1754	1746	566	101	69.4
(WY)	1983	1983	1965	1980	1982	1983	1982	1983	1983	1983	1983	1982
MIN	2.89	7.65	8.67	10.8	15.4	39	84.4	117	27	5.06	1.86	2.28
(WY)	1978	1991	1991	1991	1991	1977	1977	1977	1992	1977	1977	1977

SUMMA	RY	STATISTICS	FO	R 1992 CALENDAR YEAR	FOR 1993 WATER YEAR	WATER YEARS 1960 - 1993		
ANNUAL	L TOTAL		37162	0.1	140379	0.1		
ANNUAL	L MEAN		102		385			
HIGH	ST ANNUAL MEAN					255		
LOWES	T ANNUAL MEAN					771		
HIGH	ST DAILY MEAN		575 Apr	13	2000 Mar	17	12000 Feb	16 1982
LOWES	T DAILY MEAN		3.2 Oct	1	3.2 Oct	1	1.2 Sep	10 1977
ANNUAL	L SEVEN-DAY MINIMUM		3.3 Sep	27	3.5 Oct	1	1.3 Sep	7 1977
MAXIM	UM PEAK FLOW				2760 Mar	17	19400 Jan	13 1980
MAXIM	UM PEAK STAGE				11.58 Mar	17	21.47 Jan	13 1980
ANNUAL	L RUNOFF (AC-FT)		73710		278400		184600	
10 PE	RCENT EXCEEDS		326		1070		672	
50 PE	RCENT EXCEEDS		35		185		71	
90 PE	RCENT EXCEEDS		4	0.3	12		8	0.8

More? [Y/N DEF AULT=Y]:
 EOF[1;1H EOF[1;1H U. S. DEPARTMENT OF THE INTERIOR - U.S. GEOLOGICAL SURVEY NAME? RESOURCES

STATION NUMBER 11283500 CLAVEY RIVER BUCK MEADOWS CAMP SOURCE AGENCE USGS STATE 06 COUNTY 1 9
 LATIT UDE 375 402 LONGITUDE 1200415 NA D27 DRAINAGE AREA 144* CO NTRIBUTING DRAINAGE AREA DATUM 2374.08 NGVD29
 Date Processed: 2006-11-21 09:19 By turloc k
 Lowes Tagging Status in period is APPROVED
 DD #1
 Discharge, cubic feet per second
 WATER YEAR OCTOBER 1993 TO SEPTEMBER 1994
 DAI LY MEAN VALUES

DAY OCT NOV DEC JAN FEB MAR APR MAY JUN JUL AUG SEP

1	11	14	27	25	31	132	289	345	177	21	6.1	3.3
2	11	13	22	24	29	140	301	364	148	20	5.8	3.2
3	11	13	21	24	30	160	328	364	137	19	5.5	3.2
4	11	13	20	26	28	178	300	363	121	18	5.4	3.3
5	11	13	19	34	27	217	245	361	110	18	5.3	3.4
6	12	13	19	28	28	230	233	346	103	17	5.1	3.4
7	13	13	18	27	109	207	201	324	95	16	4.9	3.3
8	13	13	18	26	116	203	201	316	86	16	4.6	3.3
9	12	13	20	25	76	223	220	314	80	15	4.4	3.2
10	12	13	21	22	65	234	190	362	75	13	4.4	3.2
11	14	17	27	22	63	228	193	399	69	13	4.4	3.2
12	16	24	29	22	48	205	209	403	64	12	4.2	3.5
13	15	21	25	23	48	195	236	344	59	12	4	3.7
14	15	18	29	23	42	253	286	324	55	11	3.9	3.8
15	17	17	26	23	42	307	339	283	51	11	3.8	4
16	30	16	23	22	42	293	399	218	48	10	3.6	3.9
17	26	16	22	23	95	241	412	186	45	9.7	3.5	3.7
18	23	16	22	23	93	237	407	219	43	9.1	3.4	3.6
19	20	16	22	24	69	263	429	262	41	8.8	3.4	3.5
20	18	16	21	25	71	235	429	269	39	8.6	3.4	3.5
21	17	16	21	25	66	238	390	320	37	8.6	3.4	3.5
22	17	17	21	25	59	244	329	326	35	8.7	3.4	3.4
23	16	18	21	44	63	189	289	268	33	8.6	3.4	3.4
24	16	17	22	52	67	165	251	253	31	8.1	3.4	3.7
25	15	16	22	41	76	152	249	253	30	7.8	3.4	4.2
26	15	16	23	44	88	141	236	215	28	7.4	3.4	4.4
27	14	16	30	36	114	154	272	220	27	7.1	3.3	4.2
28	14	17	29	30	122	216	249	205	25	6.7	3.3	4.2
29	14	18	26	30	---	245	291	183	23	6.4	3.3	6.5
30	14	40	25	31	---	250	317	175	22	6.2	3.3	7.7
31	14	---	24	30	---	293	---	196	---	6.1	3.3	---
TOTAL	477	499	715	879	1807	6668	8720	8980	1937	359.9	126	114.4
MEAN	15.4	16.6	23.1	28.4	64.5	215	291	290	64.6	11.6	4.06	3.81
MAX	30	40	30	52	122	307	429	403	177	21	6.1	7.7
MIN	11	13	18	22	27	132	190	175	22	6.1	3.3	3.2
AC-FT	946	990	1420	1740	3580	13230	17300	17810	3840	714	250	227

STATISTICS OF MONTHLY MEAN DATA FOR WATER YEARS 1960 - 1999, 4, BY WATER YEAR (WY)

MEAN	27.1	72.9	148	267	314	426	605	687	331	84.3	22.8	17
MAX	226	339	999	1331	1426	1482	2057	1754	1746	566	101	69.4
(WY)	1983	1983	1965	1980	1982	1983	1982	1983	1983	1983	1983	1982
MIN	2.89	7.65	8.67	10.8	15.4	39	84.4	117	27	5.06	1.66	2.28
(WY)	1978	1991	1991	1991	1991	1977	1977	1977	1992	1977	1977	1977

SUMMA	RY	STATISTICS	FO	R 1993 CALENDAR YEAR	FOR 1994 WATER YEAR	WATER YEARS 1960 - 1994
ANNUAL TOTAL				139237	31282	0.3
ANNUAL MEAN				381	85	0.7
HIGHEST ANNUAL MEAN						250
LOWEST ANNUAL MEAN						771
HIGHEST DAILY MEAN				2000 Mar	17	429 Apr
LOWEST DAILY MEAN				11 Sep	28	3.2 Sep
ANNUAL SEVEN-DAY MINIMUM				11 Sep	28	3.3 Aug
MAXIMUM PEAK FLOW					537 Apr	20
MAXIMUM PEAK STAGE					6.61 Apr	20
ANNUAL RUNOFF (AC-FT)				276200	62050	180800
10 PERCENT EXCEEDS				1070	276	656
50 PERCENT EXCEEDS				175	24	69
90 PERCENT EXCEEDS				13	3	0.7
More?	[Y/N DEF AULT=Y]:					
[[HIG]]	2J0[1;1H	D[1;1H	U.	S. DEPARTMENT OF THE INTERIOR - U.S. GEOLOGICAL SURVEY NAME? RESOURCES		

STATION NUMBER 11283500 CLAVEY RIVER MEADOWS CALIFORNIA SOURCE AGENCY USGS STATE 06 COUNTY 1 9
LATITUDE 37° 40' LONGITUDE 120° 00' 45" DRAINAGE AREA 144* COASTAL MOUNTAINS DRAINAGE AREA DATUM 2374.08 NGVD29
Date Processed: 2006-11-21 09:19 By turlock
Lowest stage status in period is APPROVED
DD #1
Discharge, cubic feet per second
WATER YEAR OCTOBER 1994 TO SEPTEMBER 1995
DAILY MEAN VALUES

DAY	OCT	NOV	DEC	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP
1	6.6	8.8	57	70	494	483	699	5840	1370	—	—	—
2	5.8	12	66	60	539	491	691	—	1210	—	—	—
3	5.4	12	78	65	520	1030	728	2100	1150	—	—	—
4	19	11	102	92	508	815	864	1860	1210	—	—	—
5	61	36	105	175	503	642	972	1680	1020	—	—	—
6	27	349	102	122	499	573	998	1390	822	—	—	—
7	21	153	84	340	479	520	1570	1210	723	—	—	—
8	19	94	61	327	467	483	1410	1110	649	—	—	—
9	17	62	60	622	436	3220	1060	1110	634	—	—	—
10	16	70	58	2910	413	8150	905	1120	790	—	—	—
11	16	51	55	1530	401	4810	935	1240	891	—	—	—
12	15	49	61	847	394	2500	1040	1190	920	—	—	—
13	14	44	58	1420	387	1890	1210	1090	911	—	—	—
14	13	38	50	2930	383	1770	990	927	—	—	—	—
15	12	40	56	1740	344	1610	836	870	—	—	—	—
16	11	42	54	915	330	1430	739	860	—	—	—	—
17	11	42	55	626	314	1240	679	954	—	—	—	—
18	10	38	58	511	307	1280	646	1050	—	—	—	—
19	10	38	59	446	322	1370	610	1270	—	—	—	—
20	10	46	59	402	370	1370	608	1500	—	—	—	—
21	9.8	44	59	364	427	1340	570	1500	—	—	—	—
22	9.5	41	62	356	458	1130	570	1400	—	—	—	—
23	9.4	41	62	434	468	1090	633	1270	—	—	—	—
24	9.3	43	87	599	479	898	776	1250	—	—	—	—
25	9.1	60	83	696	491	778	970	1130	—	—	—	—
26	8.9	58	84	559	492	708	1060	1180	—	—	—	—
27	8.9	51	82	539	466	673	1340	1300	—	—	—	—
28	8.8	55	83	512	460	648	2220	1320	—	—	—	—
29	8.7	51	73	469	—	625	3440	1310	—	—	—	—
30	8.6	52	67	442	—	619	3130	1280	—	—	—	—
31	8.4	—	66	449	—	647	—	1360	—	—	—	—

APPENDIX H
Flow Records for
Marco and Polo Creeks

Application #31491
Spring Flow Recap

Marco Creek

Below POD

	<u>GPM</u>
5/24/05	— 80
7/26/05	— 60
9/21/05	— 55
5/9/06	— 85
6/5/06	— 65
7/20/06	— 60
9/20/06	— 50
5/10/07	— 55
7/16/07	— 35
10/20/07	— 20
12/4/07	— 17
5/15/08	— 20
6/24/08	— 20

"Old Railroad Grade"

	<u>GPM</u>
5/24/05	— 120
7/26/05	— 90
9/21/05	— 82
5/9/06	— 120
6/5/06	— 100
7/20/06	— 100
9/20/06	— 85
5/10/07	— 80
7/16/07	— 65
10/20/07	— 50
12/4/07	— 45
5/15/08	— 45
6/24/08	— 45

Polo Creek

Below POD

	<u>GPM</u>
5/24/05	— 70
7/26/05	— 50
9/21/05	— 35
5/9/06	— 65
6/5/06	— 55
7/20/06	— 50
9/20/06	— 45
5/10/07	— 30
7/16/07	— 20
10/20/07	— 15
12/4/07	— 12
5/15/08	— 25
6/24/08	— 15

"Old Railroad Grade"

	<u>GPM</u>
5/24/05	— 110
7/26/05	— 80
9/21/05	— 65
5/9/06	— 115
6/5/06	— 100
7/20/06	— 90
9/20/06	— 85
5/10/07	— 60
7/16/07	— 45
10/20/07	— 25
12/4/07	— 23
5/15/08	— 45
6/24/08	— 45



TOTAL P.01

APPENDIX I
Water Demand Analysis of US Forest Service Usage

Water Available Analysis U. S. Forest Service Usage

Hull Creek Campground -

21 sites X 4 person/site X 5 gal./person/camping-day X 235 camping-days/year X 40% occupancy =
= 39,480 gallons/year = 39,480 gals./325,830 gals./acre-ft. = 0.12 ac.-ft./yr.

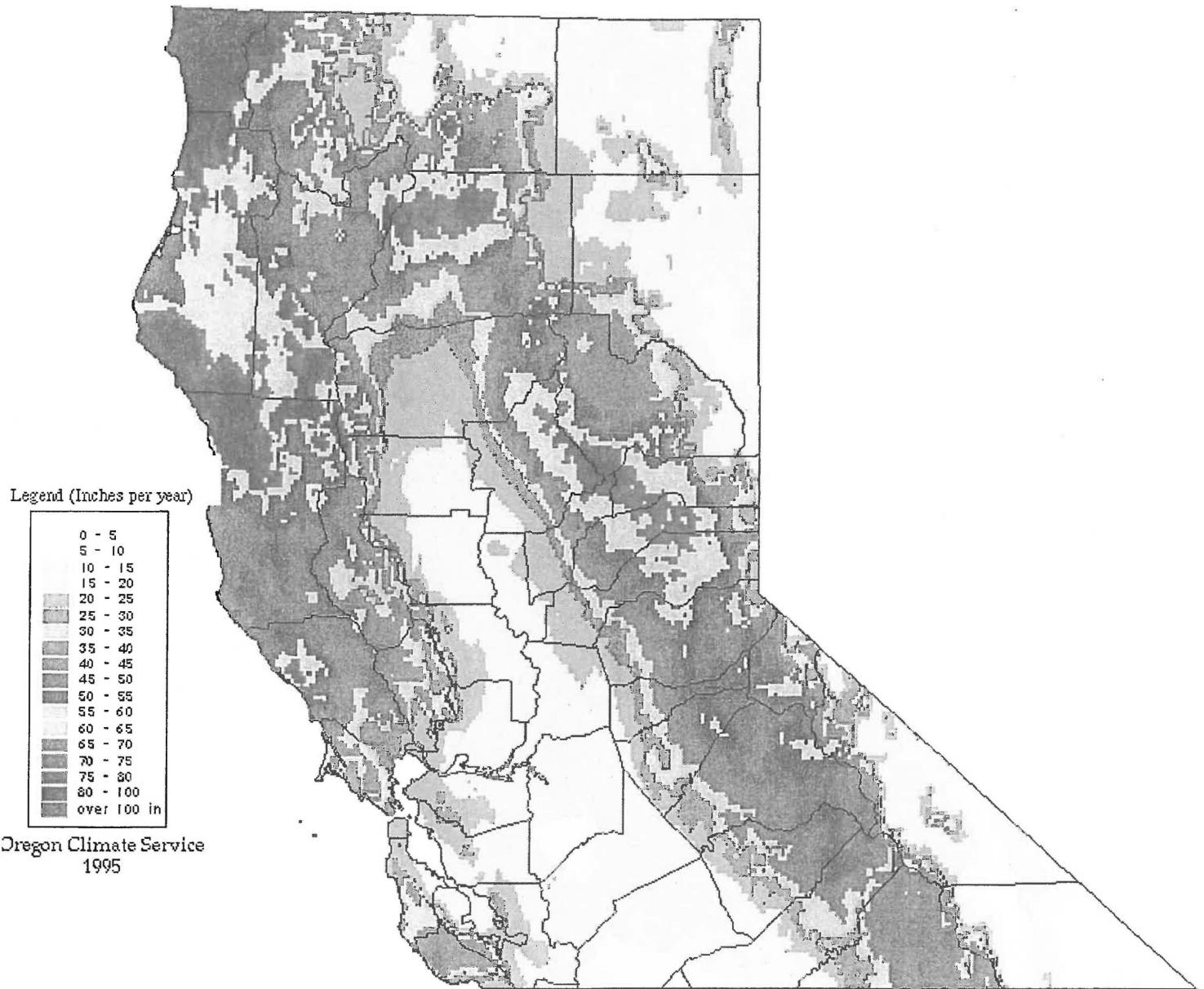
Range Cattle -

250 head-cattle X 106 days/year X 15 gals/day/head = 397,500 gals./yr. =
= 397,500 gals./yr./325,830 gals./acre-ft. = 1.22 ac.-ft./yr.

Total Reserved Right Usage

= Hull Creek Campground + Hull Creek Range Cattle
= 0.12 ac.-ft./yr. + 1.22 ac.-ft./yr.
= 1.34 ac.-ft.

APPENDIX J
Map of Annual Average Precipitation
Northern California, 1961-1990



Annual Average Precipitation (Inches),
Northern California

Period: 1961-1990